Reassessment of the intrinsic bulk recombination in crystalline silicon

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1. Introduction

In recent years, we have seen significant improvements in the electrical quality of industrially feasible silicon wafers. This was primarily driven by improved material growth and wafer manufacturing techniques and the development of processing steps to mitigate contamination giving rise to recombination in the silicon bulk. The ongoing rapid improvement of solar cell efficiencies in both research and mass-production is largely driven by further reduction of recombination at interfaces and surfaces via the improvement of passivation layers [1-8]. This has led to measured effective charge carrier lifetimes τ_{eff} significantly exceeding the most widely used parameterisation of the intrinsic limit of silicon by Richter et al. [9], as shown e.g. in Refs. [10,11]. Further improvements in solar cell fabrication processes and next generation solar cell concepts (e.g. TOPCon [12]/POLO [13]) will continue to exacerbate the need for an accurate description of intrinsic recombination predicted for moderate injection, we further revise the fundamental limiting power conversion efficiency for a single-junction crystalline silicon solar cell to 29.4%, which is within 0.1%_{abs} compared to other recent assessments.

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ABSTRACT

Characterisation and optimization of next-generation silicon solar cell concepts rely on an accurate knowledge of intrinsic charge carrier recombination in crystalline silicon. Reports of measured lifetimes exceeding the previous accepted parameterisation of intrinsic recombination indicate an overestimation of this recombination in certain injection regimes and hence the need for revision. In this work, twelve high-quality silicon sample sets covering a wide doping range are fabricated using state-of-the-art processing routes in order to permit an accurate assessment of intrinsic recombination based on wafer thickness variation. Special care is taken to mitigate extrinsic recombination due to bulk contamination or at the wafer surfaces. The combination of the high-quality samples with refined sample characterisation and lifetime measurements enables a much higher level of accuracy to be achieved compared to previous studies. We observe that reabsorption of luminescence photons inside the sample must be accounted for to achieve a precise description of radiative recombination. With this effect taken into account, we extract the lifetime limitation due to Auger recombination. We find that the extracted Auger recombination rate can accurately be parameterized using a physically motivated equation based on Coulomb-enhanced Auger recombination for all doping and injection conditions relevant for silicon-based photovoltaics. The improved accuracy of data description obtained with the model suggests that our new parameterisation is more consistent with the actual recombination process than previous models. Due to notable changes in Auger recombination predicted for moderate injection, we further revise the fundamental limiting power conversion efficiency for a single-junction crystalline silicon solar cell to 29.4%, which is within 0.1%_{abs} compared to other recent assessments.
recombination in silicon. With current passivation layers allowing for carrier lifetimes exceeding the hitherto perceived theoretical limit, both characterisation of further advancements and simulation of their exploitation are limited. Therefore, we have undertaken a long-term endeavour to create an improved description of Auger recombination [9,14]. This work presents the results of the ongoing process optimization and more than three years of silicon wafer selection and preparation as well as refinement of charge carrier lifetime characterisation. Reduction of the impact of extrinsic recombination channels to a minimum was achieved via the state-of-the-art surface passivation layers and thickness variation experiments. This allows us to reassess recombination via intrinsically limiting processes of radiative and Auger recombination with a new precision.

Due to the indirect band gap of silicon, radiative recombination is not predominant. Since an electron and a hole are involved in the process, the total rate of radiative recombination $R_{\text{rad,tot}}$ in dependence of their respective concentrations $n$ and $p$ reads

$$R_{\text{rad,tot}} = B_{\text{rad}} np$$

(1)

The coefficient $B_{\text{rad}}$ in this relation includes effects of the band structure of the silicon crystal and can be determined by luminescence rate measurements (e.g. Refs. [15,16]) or derived from band-to-band absorption measurements via the generalized Planck law [17]. One important factor incorporated in $B_{\text{rad}}$ is the effect of Coulomb interaction of the involved electron and hole – and the fact that this interaction can be screened by surrounding charge carriers [16,18]. At moderate temperatures, the transition between negligible and dominant screening occurs around the range of charge carrier densities between $10^{12}/\text{cm}^3$ and $10^{19}/\text{cm}^3$ and must therefore be taken into account carefully in any model intended for use in silicon photovoltaic applications [17]. This is usually done via an injection-dependent factor $B_{\text{rel}}$ multiplied with experimentally assessed values for $B_{\text{rad}}$ using high resistivity silicon which we denote as $B_{\text{low}}$ [15,17,19]. In this work, we account for screening via an implementation of the random-phase approximation band gap narrowing model of Schenk [20] as motivated in a recent contribution by Fell et al. [21]. We also apply the considerations of Fell et al. to determine the fraction $f_\text{ph}$ of photons emitted by radiative recombination that is reabsorbed within the sample. Since such reabsorption results in new electron hole pairs, it must be considered for precise assessment of radiative recombination.

Auger recombination describes the nonradiative recombination of an electron (e) and a hole (h) with the excess energy being transferred to a third electron or hole. Assuming the three particles to be quasi-free inside the silicon crystal, the two possible processes (referred to by the involved carriers as $\text{eh}$ or $\text{ehh}$) are considered independent and determined by the coefficients $C_{\text{eh}}$ and $C_{\text{ehh}}$ and the respective carrier concentrations $n$ and $p$. Then, the sum of the resulting rates represents the total rate of Auger recombination:

$$R_{\text{Auger,tot}} = R_{\text{eh}} + R_{\text{ehh}} = C_{\text{eh}} n^2 p + C_{\text{ehh}} np^2$$

(2)

However, previous works have established and demonstrated that Auger recombination processes in silicon are affected by interaction of the involved charge carriers with the crystal lattice and other free charge carriers [9,22-25] (and references therein). An important effect for charge carrier concentrations below $10^{17}/\text{cm}^3$ is an enhancement of Auger recombination caused by the Coulomb interactions of the charge carriers mentioned above as addressed and demonstrated by Hangleiter and Häcker [23]. Again, for high charge carrier densities, this influence is suppressed by free-carrier screening. Therefore, Auger recombination is then well-described by the simple relation suggested in eq. (2) again. In this work, the impact of Coulomb enhancement of Auger recombination is accounted for by considering enhancement factors $g_{\text{eh}}$ and $g_{\text{ehh}}$ as suggested by Hangleiter and Häcker [23] which will be discussed in section 3. The parameterisation by Richter et al. [9] included empirical terms to describe the dependence of Auger recombination on doping and injection separately. We find in retrospect that this artificial division was only necessary due to impacts of extrinsic recombination channels on the used data set.

Any measured effective charge carrier lifetime $\tau_{\text{eff}}$ describes the net recombination rate as difference of total recombination and total generation $\Delta R = R_{\text{tot}} - G_{\text{tot}}$ in a given situation. Besides extrinsic carrier injection or generation this includes equilibrium generation rates. Hence the term we apply for the lifetime limitation induced by recombination path $x$ is

$$\tau_x = \frac{\Delta n}{\Delta R_x} = \frac{\Delta n}{R_{\text{tot}} - G_x}$$

(3)

The generation term $G_x$ is equal to the respective equilibrium recombination rate and hence calculated with the equilibrium carrier densities $n_0$ and $p_0$. It is numerically negligible in most application cases.

2. Experiment

Measurements to ascertain the intrinsic charge carrier lifetime $\tau_{\text{inj}}$ require both the detection and mitigation of extrinsic recombination channels and reliable charge carrier lifetime measurements. Special care was taken to select samples and process routes to reduce recombination caused by extrinsic bulk defects, as well as reducing recombination at the sample surfaces by state-of-the-art surface passivation. The experiments and sample characterisation were designed to reduce and assess uncertainties wherever possible. This includes assessment of bulk recombination via the thickness variation method [26] to take even ultra-low surface recombination into account without any extrapolation between different materials.

2.1. Sample preparation

The most accurate method to determine bulk recombination when the diffusion length is large compared to the sample thickness is to correct for surface recombination by varying the sample thickness. Assuming that a sample set based on the same bulk material and processed together (e.g. as in Ref. [27]) will possess comparable surface passivation, variation of sample thickness allows extraction of all thickness-dependent terms [26]. This approach has been applied in a limited manner in previous parameterisations of intrinsic recombination, primarily to assess surface recombination for the used dielectric layer stacks [9,14,25]. For the present study we instead make use of a large number of thickness variation sets in order to avoid the extrapolation of surface recombination between different samples of e.g. varied doping. The investigated sample sets are listed in Table 1. The method becomes more reliable given a larger thickness range, so long as consistent material parameters and surface passivation quality can be ensured for the samples used. Thus, we fabricated several sample sets featuring systematic thickness variation (i.e. sets N100, N2.3, N1.9 and P80) by purposefully cutting them from high-purity float zone silicon (FZ Si) ingots obtained directly from the crystal grower. To extend the resistivity range and data space, further sample sets were created from materials that had been found to feature excellent bulk lifetimes in earlier studies. These further sample sets were created from thermally pretreated FZ Si wafer sets either by mechanical gridding (i.e. sets N670, N80, N1.1, P80, P1.1 and P0.5) followed by mechanical and chemical surface polishing, or by prolonged wet chemical etching (i.e. sets P0.6 and P1.5). The starting wafers were chosen carefully to originate from the same box and hence likely neighbouring parts of the same original crystal.

The thermal pretreatment was found to be necessary, since although the used FZ Si is very pure and features a high crystallographic quality, it still contains defects that can cause significant extrinsic charge carrier recombination. It has been shown in the past that thermal treatments in the typical processing temperature range between 400 and 1000 °C can increase or reduce this unwanted recombination activity [28,29].
plasma-assisted atomic layer deposition (PA-ALD) in a FlexAL via specifically optimized process routes. The used TOPCon layer stacks -

Table 1

<table>
<thead>
<tr>
<th>Set</th>
<th>Dopant</th>
<th>Resistivity at R.T. (Ωcm)</th>
<th>Samples(^a) (used/processed)</th>
<th>Thickness range(^b) [µm]</th>
<th>Passivation(^c)</th>
</tr>
</thead>
<tbody>
<tr>
<td>N1.1</td>
<td>P</td>
<td>1.09</td>
<td>7/12</td>
<td>93–425</td>
<td>TOPCon</td>
</tr>
<tr>
<td>N1.9</td>
<td>P</td>
<td>1.88</td>
<td>3/6</td>
<td>137–1414</td>
<td>TOPCon</td>
</tr>
<tr>
<td>N2.3</td>
<td>B</td>
<td>2.27</td>
<td>8/9</td>
<td>140–1437</td>
<td>TOPCon</td>
</tr>
<tr>
<td>N100</td>
<td>P</td>
<td>–100</td>
<td>2/5</td>
<td>100–1500</td>
<td>TOPCon</td>
</tr>
<tr>
<td>N80</td>
<td>P</td>
<td>–80</td>
<td>4/11</td>
<td>94–314</td>
<td>TOPCon</td>
</tr>
<tr>
<td>N670</td>
<td>P</td>
<td>–670</td>
<td>4/9</td>
<td>93–480</td>
<td>TOPCon</td>
</tr>
<tr>
<td>P0.6</td>
<td>B</td>
<td>0.6</td>
<td>4/12</td>
<td>83–272</td>
<td>Al₂O₃</td>
</tr>
<tr>
<td>P0.5</td>
<td>B</td>
<td>0.5</td>
<td>4/12</td>
<td>230–506</td>
<td>Al₂O₃</td>
</tr>
<tr>
<td>P1.5</td>
<td>B</td>
<td>1.5</td>
<td>6/12</td>
<td>82–273</td>
<td>Al₂O₃</td>
</tr>
<tr>
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<td>B</td>
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<td>5/14</td>
<td>96–546</td>
<td>TOPCon</td>
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<tr>
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<td>B</td>
<td>3.01</td>
<td>5/9</td>
<td>100–1500</td>
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<tr>
<td>P90</td>
<td>B</td>
<td>–30</td>
<td>3/2</td>
<td>93–290</td>
<td>TOPCon</td>
</tr>
</tbody>
</table>

\(^a\) P: phosphorus, B: boron.

\(^b\) A larger sample set was processed and only samples with excellent passivation were picked for the final evaluation. The given thickness range refers to the used samples.

\(^c\) See Appendix A section for processing details.

occurrence of these defects is usually indicated by a characteristic pattern of lateral lifetime non-uniformity where the central area of the wafers is more affected. The defect occurrence can be avoided by the application of high process temperatures [28,30]. In a reassessment of the sample set used by Richter et al. for the previous parameterisation [9], we observed that some of the wafers showed a faint defect signature when characterised by photoluminescence imaging (PLI), indicating an extrinsic limitation. To avoid this detrimental impact on the new parameterisation, the wafers in this study underwent a specific process route including a thermal oxidation and external gettering step developed in a previous work of the author consortium [10]. All fabricated samples were passivated with state-of-the-art surface passivation layers via specifically optimized process routes. The used TOPCon layer stacks were optimized for optimum surface passivation as discussed in Ref. [27]. The aluminium oxide layers were deposited via plasma-assisted atomic layer deposition (PA-ALD) in a FlexAL™ reactor, as discussed in Ref. [14]. For a more detailed overview on the applied processes the reader is referred to the Appendix section A where Fig. 5 shows a flow chart of the processing routes.

Besides the specifically processed sample sets, additional passivated wafers were provided by an industry partner. These wafers from Czochralski-grown n-type silicon wafers cover the resistivity range of 1.4 to 0.18 Ω cm and were especially useful to extend the n-type doping range to concentrations above 10^{16} cm⁻³. The samples were all of similar thickness and hence the direct extraction of bulk lifetimes was not possible.

2.2. Sample overview

Table 1 holds an overview on the sample sets processed for this work. More information on the sample processing — including a process flow sketch — is included in the Appendix section A.

2.3. Lifetime measurement

Most wafers were subjected to spatially resolved photoluminescence imaging characterisation in a modulum tool [31] to identify the region on the sample least affected by local flaws in surface passivation or handling damage. This imaging setup allows for in situ lifetime calibration of PLI and hence diffusion length assessment, which was helpful to identify samples not suitable for further analysis due to extrinsic effects such as sample handling induced damage.

The characterisation of the total recombination τ₉₀₀ as a function of Δn in each sample was performed by photocconductance decay (PCD) measurements using Sinton Instruments WCT-120 lifetime testers carefully calibrated to account for sample thickness [32] (see also calibration data in the Appendix C). Both measurement modes — i.e. with short and long flashes were recorded for all samples. The available injection level range of the gathered charge carrier lifetime curves τₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑᵉ степени

2.4. Lifetime data evaluation

Multiple lifetime measurements were performed for each sample with varied measurement parameters. Besides self-consistent transient PCD measurements we also performed measurements featuring a slow-decaying flash. Due to the high quality and lateral homogeneity of the samples it was possible to assess the optical factors f₉₀₀ necessary for the generalised evaluation of such measurements from direct comparison to transient lifetime data. The determined values for f₉₀₀ were consistent on most sample sets. When unexpected variations in the optical factor of more than 0.05 were observed, the respective measurements were given less weighting in the final fit to the data. As discussed in the recent contribution by Black and Macdonald [34] the common approach of PCD measurement evaluation provided by the current Sinton Lifetime tester software is not precise in certain charge carrier concentration regimes. Following the suggestions in Ref. [34] we therefore evaluated the raw data with our own purpose-built software, which makes use of the Klaassen mobility model [35,36] to determine the time-dependent excess charge carrier density Δn(t) from the measured total sample conductance σ(t). A 2-point centralized derivative was used for assessment of the transient terms of carrier decay [37]. Measurement noise and electronic artefacts were removed as outlined in the Appendix (Section C).

2.4.1. Measured effective charge carrier lifetimes

The thickness variation experiments performed for this work were found to feature excellent effective charge carrier lifetimes τₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑᵉ степени

2.4.2. Extraction of bulk lifetime

In order to assess intrinsic limitation, we need to distinguish the recombination channels that are incorporated within the measured τₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑₑᵉ степени

3


Fig. 1. Measured lifetimes and extracted lifetimes for the thickness variation sample sets N670 (a) and N2.3 (b). The dashed horizontal lines illustrate the highest measured $\tau_{\text{rel}}$ used to include the measurements in the record lifetime comparison graph in Fig. 8 in the Appendix. The surface recombination velocity extracted from the measurement series is shown in Fig. 9 in the Appendix.

$$
\tau_{\text{eff}}(W) = \left( \frac{1}{\tau_{\text{bulk}}} + \frac{1}{\tau_{\text{surface}}(W)} \right)^{-1} = \left( \frac{1}{\tau_{\text{bulk}}} + \frac{2R_{\text{surface}}}{W} \right)^{-1}
$$

(4)

$$
\tau_{\text{bulk}} = \lim_{W \to \infty} \left( \tau_{\text{eff}}(W) \right)
$$

(5)

This evaluation assumes $\tau_{\text{bulk}}$ and recombination at the wafer surfaces $R_{\text{surface}}$ to be the same for all samples of one set. Then, a linear relation is expected between $(\tau_{\text{rad}})^{-1}$ and $1/W$ and the extrapolation to $1/W = 0$ (i.e. $W = \infty$) can be used to extract $\tau_{\text{bulk}}$. The linearity can also help to assess the validity of extracted bulk lifetimes. Our processing routes were designed to reduce extrinsic bulk recombination to a minimum and otherwise ensure that potential remaining limitations would be comparable in the samples of each set. However, direct extraction of $\tau_{\text{bulk}}$ from $\tau_{\text{eff}}$ with eq. (5) would just be an approximation because there is a difference in the impact of radiative recombination between the samples. As suggested by Kerr et al. [39] and discussed further by Fell et al. [21], the reabsorption of radiatively emitted photons inside the sample cannot be assumed independent of sample thickness and surface condition. For planar samples the significant total internal reflection of many photons means that >80% of photons are reabsorbed within the sample itself. Reabsorption can occur via intra-band absorption of free carriers, referred to as free carrier absorption (FCA), or via band-to-band absorption. The latter effect is termed photon recycling (PR) and creates free electron-hole pairs with rate $G_{\text{PR}}$. Since $G_{\text{PR}}$ is directly linked to the rate $R_{\text{rad, tot}}$ it can be accounted for by a term $(1-f_{\text{PR}})$ to be

$$
R_{\text{rad, tot}} = R_{\text{rad, tot}} \cdot (1 - f_{\text{PR}}) = B_{\text{low}}B_{\text{rel}}(\Delta n) \left( 1 - f_{\text{PR}} \right) \frac{n}{p}
$$

(6)

The fraction $f_{\text{PR}}$ of reabsorbed photons in every sample was assessed via the analytical model described in Ref. [21] taking FCA into account. Appendix section F contains a polynomial approximation for $f_{\text{PR}}$ of typical sample structures. It should be noted that FCA and PR are competing processes and therefore precise modelling of radiative recombination in highly injected silicon should take FCA into account to accurately assess $f_{\text{PR}}$.

We subtract $R_{\text{rel, tot}}$ from each $R_{\text{eff}} = 1/\tau_{\text{eff}}(\Delta n)$ curve prior to the evaluation of the thickness-dependent sample sets. Thus, we can directly isolate $\tau_{\text{Auger}}$ which is the dominant intrinsic recombination source in silicon under most circumstances. For this purpose, we applied the low-carrier-density-limit of the radiative recombination coefficient $B_{\text{low}}$ of $4.76 \times 10^{-15} \text{ cm}^{-6}$ determined by Nguyen et al. [15] multiplied by $B_{\text{rel}}$ calculated via the band gap narrowing model of Schenk [20] to account for Coulomb screening, as introduced in Ref. [21].

The resulting extracted $\tau_{\text{Auger}}(\Delta n)$ for the twelve thickness-dependent sample sets are shown in Fig. 2a. Excellent lifetime levels at low charge carrier densities are observed, and the lifetimes are comparable to or above previously reported record lifetimes. The direct comparison of the curves shows all curves tend to converge at high injection densities. This illustrates an improved consistency of measurement data quality compared to Ref. [9], since $\tau_{\text{Auger}}$ of highly-injected silicon is expected to coincide for p- and n-type doping.

An extraction of $\tau_{\text{Auger}}$ with the approach described above was not possible for the additional n-type samples of high doping concentration due to the single wafer thickness. Therefore, the $\tau_{\text{eff}}$ were corrected for radiative recombination and a reasonable surface recombination of 0.5 $\text{fa/cm}^2$. This assumption results in a lower reliability of $\tau_{\text{Auger}}$ and was accounted for by a reduced weight in the subsequent fit.

3. Parameterisation of intrinsic recombination

For the description of the lifetime limitation via Auger recombination we apply

Fig. 2. a) Extracted Auger lifetime limitations $\tau_{\text{Auger}}$ for the investigated thickness-dependent sample sets. The lines indicate the parameterisation of Auger recombination suggested in this work as evaluated with eq. (7) and the parameters given in Table 2 b) Relative deviation of the experimentally extracted $R_{\text{Auger}}$ from the suggested model with the grey area indicating 20% deviation. The plot shows the part of the original data that was used for the final fit.
\begin{align}
    \tau_{\text{Auger}} &= \frac{\Delta n}{C_{\text{eeh}} \Delta n \left( N^p p - N^h p \right) + C_{\text{ehh}} \Delta n \left( N^p n + N^h n \right)} - \frac{\Delta n}{\Delta R_{\text{Auger}}} \quad (7)
\end{align}

A parallel publication by Black and Macdonald [34] reviews literature data on Auger recombination in highly-doped silicon. It is discussed that the commonly used Auger coefficients \( C_{\text{eeh}} \) and \( C_{\text{ehh}} \) by Dreiziger and Schmid [40] need to be corrected using up-to-date mobility models. To achieve a good description of the corrected data, Black and Macdonald suggest values of \( C_{\text{eeh}} = 3.41 \times 10^{-31} \text{ cm}^{-6}\text{s}^{-1} \) and \( C_{\text{ehh}} = 1.17 \times 10^{-31} \text{ cm}^{-6}\text{s}^{-1} \). We adapt these values for our parameterisation, because this work does not report new data points for the high doping concentrations, where \( C_{\text{eeh}} \) and \( C_{\text{ehh}} \) can best be determined.

The terms \( g_{\text{eeh}} \) and \( g_{\text{ehh}} \) were introduced to reflect Coulomb enhancement due to the interactions of unscreened charge carriers. They are functions of charge carrier density and describe the transition between pronounced Coulomb enhancement for low carrier concentrations to its absence at higher concentrations. There is no simple analytical expression for the effect of the three-particle interaction [23]. Therefore we investigated the different approaches chosen in previous works, e.g. Refs. [9,22,24,34,41]. In analogy to the work of Black and Macdonald we chose to adopt the empirical formalism suggested by Jonsson et al. [41] which we restructured and changed to account for the sum of both carrier concentrations to provide a more coherent behaviour for highly-doped silicon [25]. The expression for \( g_{\text{eeh}} \) we used to describe our data is

\begin{align}
    g_{\text{eeh}} = 1 + \left( g_{\text{eeh,max}} - 1 \right) \frac{1}{1 + \left( \frac{\Delta n}{\Delta n_{\text{ref}}} \right)^{g_{\text{eeh}}}} \quad (8)
\end{align}

with ‘\( x \)’ standing for e and h, as appropriate. We adopt the empirical exponent \( g_{\text{Auger}} = 2 \) used by Jonsson et al. since it appears to provide a good description of the transition region. We tested different values for the Mott transition density \( N_{\text{Mott}} \) and found good agreement with literature data and our data for a value of \( 4 \times 10^{17} \text{ cm}^{-3} \). Above values of \( \sim 3 \times 10^{17} \text{ cm}^{-3} \) the choice of \( N_{\text{Mott}} \) mostly impacts description of literature data whose quality we do not reassess and therefore our choice is mainly motivated to achieve consistency with literature data and the previous parameterisation of Richter. The two Coulomb-enhancement magnitude factors \( g_{\text{eeh,max}} \) and \( g_{\text{ehh,max}} \) were consequently used as the only free fit parameters in our Auger model. Our fitting routine indicates that reasonable fits can be achieved with the assumption of equal factors \( g_{\text{eeh,max}} = g_{\text{ehh,max}} \). While the implication of identical screening behaviour for both carrier processes is interesting, we decided to exploit the additional freedom of an improved fit quality, and find an improved accuracy with values of \( g_{\text{eeh,max}} = 4.38 \) and \( g_{\text{ehh,max}} = 4.88 \). It should be noted that this implies Coulomb enhancement for low injection significantly smaller than suggested in literature [23,24]. The final parameterisation is in good agreement with the one suggested by Black and Macdonald [34]. An especially good agreement is observed when it comes to the ambipolar Auger coefficient they determined at injection densities of pronounced Coulomb-enhancement \( C_{\text{eeh,CE}} = C_{\text{eeh}} g_{\text{eeh}} + C_{\text{ehh}} g_{\text{ehh}} \) to be \( 2.11 \times 10^{-30} \text{ cm}^2\text{s}^{-1} \) - which is within \( 2\% \) of our finding. Fig. 2 illustrates the description of the \( \tau_{\text{Auger}}(\Delta n) \) data set extracted from thickness-dependent measurements.

The combination of this improved description of Auger recombination with a consistent description of radiative recombination allows for more precise modelling of the intrinsic lifetime limitation in silicon.

\begin{align}
    \tau_{\text{int}} \approx \frac{\Delta n}{\Delta R_{\text{Auger}} + \Delta R_{\text{Rad}}} \quad (9)
\end{align}

Due to the effect of PR on radiative recombination, this theoretical intrinsic lifetime cannot directly be observed with most measurement methods. For the description of experimentally assessable charge carrier lifetime we suggest using the term

\begin{align}
    \tau_{\text{int,exp}} \approx \frac{\Delta n}{(\eta_p) (C_{\text{eeh}} g_{\text{eeh}} n + C_{\text{ehh}} g_{\text{ehh}} p + B_{\text{eeh}} - B_{\text{ehh}} (1 - f_{\text{PR}}))} \quad (10)
\end{align}

in conjunction with eq. (8) and the information from Table 2. The graphs in Fig. 3 compare the model to the highest reported charge carrier lifetimes in silicon from this work, our previous work [10], and literature.

The given model is valid for a sample temperature of 300 K. Many applications of the model will likely not require accurate knowledge of \( f_{\text{PR}} \) because radiative recombination plays a minor role compared to extrinsic and Auger recombination. Thus, a precise value of \( f_{\text{PR}} \) will be of minor importance in many assessments of effective carrier lifetimes. For convenience, simple polynomial estimations of \( f_{\text{PR}} \) for two common cases – mirror-like reflection at planar surfaces and diffuse scattering at textured surfaces – are given in appendix section F. Notably, for the case of mirror-like planar surfaces, \( f_{\text{PR}} \) is very high (i.e. about 0.9 with little dependence on sample thickness). This means that neglecting radiative recombination entirely (i.e. assuming \( f_{\text{PR}} = 1 \), thus \( \tau_{\text{int,exp}} \approx \tau_{\text{Auger}} \)) in such samples may be a better assumption than not considering PR. For more detailed discussion of the relevance of reabsorption and an approach to determine it for given samples the reader is referred to Ref. [21].

A discussion of the measurement uncertainties of the used data is included in the appendix. The impact of uncertainty of parameters like sample resistivity and thickness as well as potential lateral in-homogeneity on the lifetime data – and hence the parameterisation – could not fully be assessed. The reader is referred to Fig. 2b) which demonstrates that the extracted \( R_{\text{Auger}} \) data of all materials agree well with a confidence interval of \( \pm 20\% \) to modelling using the suggested parameters (given in Table 2).

### 3.1. Impact on derived parameters

It should be kept in mind that since the new model predicts different recombination rates than previous ones this implies a change in derived parameters such as surface recombination saturation currents \( J_0 \). Where the new parameterisation predicts higher \( \tau_{\text{int}} \) – for example around 1 \( \Omega \)cm n-type – an evaluation of the same measured \( \tau_{\text{int}} \) will yield higher \( J_0 \) and vice versa. The new parameterisation also predicts significantly different intrinsic recombination compared to Ref. [9] for highly-doped silicon, as shown in Fig. 9 in Appendix section E. This change is caused by the revision of literature data suggested by Black and Macdonald [34] and the resulting \( C_{\text{eeh}} \) and \( C_{\text{ehh}} \) as well as the different form of the parameterisation formula. The changed behaviour significantly impacts the simulation of \( J_0 \) for highly-doped surfaces for which the contribution of Auger recombination is often substantial. Particular care needs to be taken when using existing parameterizations of surface recombination velocities from literature, e.g. Refs. [47,48], or the band-gap narrowing model by Yan and Cuevas [49] within such simulations, as those parameterizations have been derived from experiments using [9].

### Table 2

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Value/Model</th>
<th>Reference</th>
</tr>
</thead>
<tbody>
<tr>
<td>( C_{\text{eeh}} )</td>
<td>( 3.41 \times 10^{-33} \text{ cm}^2\text{s}^{-1} )</td>
<td>[34]</td>
</tr>
<tr>
<td>( C_{\text{ehh}} )</td>
<td>( 1.17 \times 10^{-33} \text{ cm}^2\text{s}^{-1} )</td>
<td>[34]</td>
</tr>
<tr>
<td>( g_{\text{eeh}} )</td>
<td>eq. (8) with ( g_{\text{eeh,max}} = 4.38 ) \text{This work}</td>
<td></td>
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<tr>
<td>( g_{\text{ehh}} )</td>
<td>eq. (8) with ( g_{\text{ehh,max}} = 4.88 ) \text{This work}</td>
<td></td>
</tr>
<tr>
<td>( N_{\text{Mott}} )</td>
<td>( 4 \times 10^{17} \text{ cm}^{-3} ) (for use in eq. (8)) \text{This work}</td>
<td></td>
</tr>
<tr>
<td>( \Delta \tau_{\text{Auger}} )</td>
<td>2 (for use in eq. (9))</td>
<td>[41]/This work</td>
</tr>
<tr>
<td>( B_{\text{eeh}} )</td>
<td>( 4.76 \times 10^{-15} \text{ cm}^2\text{s}^{-1} )</td>
<td>[15]</td>
</tr>
<tr>
<td>( B_{\text{ehh}} )</td>
<td>Model of Coulomb enhancement</td>
<td>[17]/[20,21]</td>
</tr>
<tr>
<td>( f_{\text{PR}} )</td>
<td>Optical model of given sample/cell</td>
<td>[21]/Appendix of this work</td>
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</table>
4. Reassessment of the theoretical limit of silicon solar cell efficiency

The improved model for intrinsic recombination leads to a change in the theoretical limit for the power conversion efficiency of single-junction crystalline silicon solar cells, which is therefore reassessed in this section. The limit was reassessed in a work by Schäfer and Brendel [50], which adjusted the calculations by Richter et al. [51] to improve the description of Lambertian light-trapping, resulting in an efficiency limit of 29.57%. More recently, an updated Auger parameterisation for n-type material was used in the same modelling approach, resulting in an efficiency limit of 29.47% [14]. For the ideal efficiency simulations in this work we use the solar cell simulation software Quokka3 [52], which employs up-to-date material models for intrinsic carrier density and carrier mobility, as well as the light-trapping and photon-recycling model described in Ref. [21]. Compared to Refs. [14,50,51], Quokka3 uses more recent models for the optical properties of silicon, namely [53] for the hand-to-hand absorption coefficient, and [54] for FCA. Furthermore, the 1D simulations include transport losses in the silicon bulk. As of writing this manuscript, Quokka3 does not account for FCA of excess charge carriers. We find that all these individual model deviations have only a marginal impact on the calculated efficiency: a close match with ~0.01% difference between our simulations and the results of [50] is found when using the Richter model for the intrinsic lifetime. This also indicates that the light-trapping and photon recycling model implemented in Quokka3 are equivalent to the accurate Lambertian limit in Ref. [50].

The maximum efficiency is obtained for undoped silicon with a thickness of ~100 μm, for which the carrier density at maximum power point is ~6 x 10^{15} cm^{-3}. At this injection level the improved Auger model of this work predicts a significantly higher recombination compared to Richter [9] resulting in a slight reduction of the efficiency limit to 29.4% (V_{oc} = 757 mV, J_{sc} = 43.4 mA/cm², FF = 89.5%). Notably, despite several differences in model assumptions, all recent publications on efficiency limits deviate only insignificantly in the range from 29.4% to 29.6%.

In Fig. 4 the limiting efficiency for undoped, as well as 1 Ωcm n-type and p-type material are plotted as a function of cell thickness, comparing Richter’s [9] and this work’s parameterisation. It can be seen that the impact of doping on the efficiency limit has become significantly less with this work’s reassessment of Auger recombination.

5. Conclusion

We have presented our work to improve the knowledge on, and description of intrinsic recombination processes in silicon samples of moderate doping and injection as relevant for solar cells. A large set of carefully chosen samples has been processed with state-of-the-art process routes to minimize the impact of extrinsic recombination. Effective charge carrier lifetimes were measured by photoconductance decay measurements. This resulted in record lifetimes of up to 0.5 s as reported in Ref. [33]. The impact of surface recombination was removed by employing the thickness variation method to extract the bulk lifetime. Radiative recombination was assessed with the parameters of Nguyen et al. [15] and the effects of photon recycling and Coulomb enhancement taken into account via optical modelling of the samples according to the suggestions by Fell et al. [21]. We find that a precise assessment of the intrinsic lifetime limit requires assessment of photon recycling effects and hence depends on the specific sample morphology. A simple polynomial estimation is given in the appendix of the paper but for a more precise description we refer to Fell et al. [21].

The remaining recombination was assessed in terms of Coulomb-enhanced Auger recombination as suggested by Hangleiter and Höcker [23]. We observe that our data are in good agreement with a simple expression for Auger recombination. The effect of charge carrier screening was taken into account via a term suggested by Jonsson et al. [41] modified to account for the carrier concentration sum. With this
adjustment, Coulomb enhancement for electrons and holes can be described by the same physical model and appears to be less pronounced than anticipated in literature. For highly doped or highly injected silicon, we based our model on recently reassessed literature data and the considerations proposed by Black and Macdonald [34]. The resulting model for Coulomb-enhanced Auger limitation is thus based on a description of the fundamental recombination process.

In conjunction with recent considerations on radiative recombination, the updated intrinsic lifetime model will improve the accuracy of simulating high-efficiency solar cells and the investigation of high purity silicon materials and state-of-the-art surface passivation layers. We applied the new model and found that the limiting efficiency of ideal single-junction crystalline silicon solar cells is 29.4%, which deviates only slightly from other recent assessments.

CRediT authorship contribution statement

T. Niewelt: Conceptualization, Investigation, Formal analysis, Data curation, Writing – review & editing. B. Steinhauser: Conceptualization, Data curation, Formal analysis, Investigation, Methodology, Resources. B. Fell: Validation, Visualization, Writing – review & editing. A. Richter: Validation, Visualization, Writing – review & editing, Resources, Methodology, Investigation, Data curation, Conceptualization. B. Veith-Wolf: Investigation, Data curation, Methodology, Resources, Writing – review & editing. A. Black: Methodology, Resources, Writing – review & editing. J. Schmidt: Funding acquisition, Conceptualization. S.W. Glunz: Conceptualization, Funding acquisition, Project administration, Supervision, Writing – review & editing. J. Tan: Resources. A. Youssef: Resources. J.D. Murphy: Writing – review & editing, Funding acquisition, Conceptualization. M.C. Schubert: Conceptualization, Writing – review & editing, Supervision, Project administration, Funding acquisition. T. Niewelt et al.

APPENDIX

A. Sample Processing

An overview of the processing schemes can be found in Fig. 5. The processes whose thermal budget can be expected to have the most relevant impact on material quality are the oxidation and phosphorus diffusion gettering processes at and above 850 °C. Each of the processes featured 60 min at the stated temperature followed by cooldown in the furnace to temperatures around 600 °C. The processes used for TOPCon passivation are described in more detail in Ref. [27]. The deposition of aluminium oxide via PA-ALD was performed in a OpAL™ reactor for the “ALox” group. More details on the latter process can be found in Ref. [14]. The passivation layers were fully activated via annealing at 425 °C in forming gas or a nitrogen atmosphere for 25 min.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Fig. 5. Process flows of the different sample sets. Grey fields indicate the processes to define sample thickness, red fields indicate thermal pre-treatments to dissolve grown-in defects [10, 28, 29, 55], blue fields indicate processes to passivate the sample surfaces, as discussed in Refs. [14, 27].

B. Sample Characterisation

The sample thickness was determined on the lifetime samples via a photogrammetric approach allowing for good precision even on samples with irregular shapes (e.g. broken-off edges). The weight of each sample was measured using precision lab scales and the wafer area taken from wafer specification or determined using scale-calibrated photographs taken with a modulum PLI setup. With the camera mounted perpendicular over the samples we estimate that the area determination using a threshold-based image analysis results in less than 2% area uncertainty. The approach provides the average thickness of the whole sample, which may differ from the spots analysed in later measurements. Thickness gauge measurements of the sample thickness were used as a consistency check. Sample sets N670, N80, N1.1, P80, P1.1 and P0.5 were created via mechanical grinding using a commercial service which should provide parallel wafer surfaces or negligible angles. Sample sets N100, N2.3, N1.9 and P3.0 were created in an industrial wire-cutting setup where individual wire slots were left out to create thicker samples. A statistical analysis of inline thickness measurements in a MeyerBurger HE-WIS-06 wafer inspection tool on >750 standard wafers cut alongside set P3.0 observed average total thickness variations of 7.1 μm. Wire cutting usually creates wedge-shaped inhomogeneity thus we assume the thickness variation across the ~3 cm in diameter lifetime measurement spot to amount to 1.8 μm. Sample sets P0.6 and P1.5 were created by prolonged etching in KOH. This process can give rise to lateral inhomogeneity due to bath convection. Therefore, the thickness of the resulting samples was also analysed locally by using a thickness gauge.

The sample doping was determined from wafer resistivity measurements performed at different stages and locations on the wafers. The resistivity measurement of the Sinton Instruments Lifetime Tester during lifetime characterisation itself is influenced by the presence of the used passivation layers. Conductive layers such as the TOPCon stack or band bending caused by fixed charges within the Al₂O₃ can affect the total resistivity especially for thin samples of low resistivity bulk material. Similar to the extraction of bulk lifetimes it was found feasible to determine bulk resistivity of moderately-doped materials by evaluation of the sheet conductance change with sample thickness. Otherwise, selected samples were etched back to silicon after lifetime characterisation to allow for bulk resistivity measurements with the inductive coil, four-point-probe measurements and electrochemical capacitance-voltage (ECV) profiling.

C. Lifetime Measurements

The WCT-120 lifetime tester used for most charge carrier lifetime measurements in this work was calibrated using a large set of wafers with different thickness and resistivity. Stacks of these wafers with different permutation were used to cover a wide range of measured voltages, as shown in Fig. 6. The calibration parameters were determined following the formalism given in Ref. [32] to calculate the apparent sheet conductance $S_{ap}$ of each wafer stack using the Sinton Lifetime tester calibration software version 5.1.
Individual lifetime measurement curves were found to be affected by various types of artefacts. Some of these occur randomly and then affect a subset of data points from the measurement. Others such as oversaturation of the measurement signal for thick samples upon strong carrier injection occurred systematically. Furthermore, a slight impact of measurement signal noise was observed. The impact of noise is most pronounced in the low carrier concentration part of the curve, where weak signals are measured, and hence small signal artefacts have a strong impact. The $\tau_{\text{eff}}(\Delta n)$ curves resulting from repeated measurements were combined as follows: injection ranges exhibiting visible scatter, oscillations, jumps or kinks were discarded; subsequently, the 5–20 curves measured per sample were plotted together and curve parts were discarded when they significantly deviated from the overall trend; when the lifetime exhibited a clear maximum, the curves were only evaluated for excess carrier densities exceeding this maximum. The resulting set of partial measurement curves was interpolated and smoothed using a monotone piecewise cubic algorithm [56]. The interpolation step serves to account for fluctuations between the measurements and simplifies the subsequent comparative evaluation for the extraction of $\tau_{\text{bulk}}$ from the thickness variation. Fig. 7 illustrates the data selection process and the extracted curves on a sample from set P80. It also shows the impact of reevaluating the raw data using a custom script with improved mobility model and differentiation algorithm.

To again illustrate the necessity of the given reparameterization of intrinsic recombination, Fig. 8 shows a direct comparison of measured lifetimes $\tau_{\text{eff}}$ from this study and earlier works to the Richter parameterisation [9].
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Fig. 8. Collection of highest measured effective lifetimes on p- and n-type doped samples [9,10,14,22,42,43]. The measured $\tau_{\text{eff}}$ were determined at different injection conditions. The lines were calculated with the Richter model and hence illustrate the necessity for an updated parameterisation of intrinsic recombination.

D. Bulk lifetime extraction assessment

As given in eq. (5) the evaluation of the thickness variation allows for extraction of bulk lifetime from the x-axis intercept of plotting recombination rate vs. inverse thickness. Evaluation of the slope yields the surface recombination velocity $S_{\text{eff}}$ for the sample set at every analysed injection density. Since it is a better quantity to compare surface recombination on differently doped samples, we analysed the $S_{\text{eff}}(\Delta n)$ curves in terms of a surface recombination current $J_{0,s}$. It was fitted to the injection density range $5 \times 10^{14} - 5 \times 10^{15}$ cm$^{-3}$ using

$$S_{\text{eff}} = \frac{J_{0,s}(N_{\text{dep}} + \Delta n)}{q n_{i,0}}$$

(11)

with the elementary charge $q$ and $n_{i,0}$ being the effective intrinsic carrier density in dark equilibrium. We did not use the resulting $J_{0,s}$ in our subsequent evaluation but it serves as quality control of the used passivation layers and sanity check for our data refinement. As expected, the used surface passivation schemes feature low surface recombination current densities around 1 fA/cm$^2$. It should be noted here that a quantitative comparison to literature data may be distorted as most values in literature were extracted from single samples using the method of Kane and Swanson [57] and necessarily have applied corrections for intrinsic recombination outdated by this work. Example curves for the description of the injection dependence of surface recombination are shown in Fig. 9. The deviation of $S_{\text{eff}}(\Delta n)$ from the theoretical curve was considered to decide which part of the data was fitted.

Fig. 9. Evaluation of surface recombination for the sample sets shown in Fig. 1. The indicated $J_{0,s}$ curve was calculated according to eq. (11) and serves as supporting evidence that I) most surface recombination is effectively suppressed by the used surface passivation and II) the thickness dependent evaluation gave plausible results. The $J_{0,s}$ values were not used for our further evaluation.
E. Fit assessment

The parameterisation of Auger processes suggested in this work was fitted to refined measurement data and is thus highly impacted by measurement uncertainty and systematic errors.

The uncertainty of lifetime assumed during fitting was largely based on reproducibility errors during \( \tau_{\text{bulk}} \) extraction from the thickness variation experiments. The nominal uncertainty of PCD lifetime measurements with the Sinton lifetime tester has been given as \( \pm 11\% \) for transient and \( \pm 8\% \) for quasi-steady-state evaluation [58]. That was based on an inter laboratory round robin experiment and a smaller intra laboratory standard deviation was observed. The study focused on the comparison of fixed-injection lifetimes but also reported derived \( J_0 \) values that indicated potential additional errors for injection dependent lifetimes. Since the round robin study [58] and the more fundamental investigation by McIntosh and Sinton [59] were performed prior to crucial measurement protocol updates (e.g. Ref. [32]) we do not consider them directly applicable to assess the uncertainty of our data and hence the derived parameterisation. The complex impact of uncertainty of sample resistivity and thickness as well as potential lateral inhomogeneity on the lifetime data could not fully be assessed. In principle, the discussion given by McIntosh and Sinton in Ref. [59] may be applied to assess the various impacts – but a full comprehensive consideration was beyond the scope of this work.

Since the model we chose to describe Auger recombination is fairly simple and contains few free fit parameters we apply a reverse approach to assess the validity of the model. Fig. 2a) shows the fit in comparison to the lifetime data. A good overall agreement is observed, especially considering that the data spans across multiple orders of magnitude in both carrier densities and lifetime. To estimate the uncertainty of the model the reader is referred to Fig. 2b) which shows the relative deviation of the \( R_{\text{Auger}}(\Delta n) \) data normalized from the suggested model. The shaded area marks an uncertainty of \( \pm 20\% \) and covers most measurement data – indicating this to be a reasonable upper limit uncertainty for the parameterisation. In this context, positive deviations are not necessarily problematic since they could be caused by unconsidered bulk recombination or an underestimated surface recombination. Extrinsic limitation in our samples – be it caused by extrinsic bulk defect recombination, laterally inhomogeneous surface passivation or other effects – reduces the measured \( \tau_{\text{eff}} \) and thus likely ends up causing a deviation from the \( T_{\text{Auger}} \) model. Such limitations would be more pronounced at low injection levels due to the strong dependence of intrinsic recombination on carrier density.

A direct comparison of the proposed model to the models of Richter et al. [9] and Black and Macdonald [34] is shown in Fig. 9. It shows good overall agreement with the model by Black and Macdonald – which was to be expected since both models use the same formalism and some key assumptions are incorporated in both parameterisations. Except in the transition region defined by the different values for \( N_{\text{eff}} \) the deviation between the models is less than 5%. Comparison to the model of Richter et al. shows more severe changes. The reports of measured \( \tau_{\text{eff}} \) exceeding \( \tau_{\text{Richter}} \) on n-type wafers in literature indicated underestimation of intrinsic recombination in this model. However, the considerations on photon recycling in this work indicate that there actually was an overestimation of \( R_{\text{rad}} \) in the work of Richter, leading to the drastic differences in \( R_{\text{Auger}} \) shown in Fig. 10. This may increase the relevance of the new parameterisation for the modelling of emitter saturation currents \( J_0 \) even further. The grey curves for undoped silicon illustrate a fundamental difference between the work of Richter and the new models suggested by Black and Macdonald and in this work. The Coulomb screening as described by eq. (8) incorporates the assumption that a symmetric charge carrier plasma (e.g. in highly injected silicon) would also suppress Coulomb enhancement.

![Fig. 10. Relative difference between the Auger recombination rate \( R_{\text{Auger}} \) predictions of the models by Richter et al. [9] and Black and Macdonald [34] to the model presented in this work. For p- and n-type doping \( \Delta n = 10^{16} \text{ cm}^{-3} \)](image)

F. Simple Photon Recycling

As discussed above, photons emitted via radiative recombination in the silicon bulk can be reabsorbed within the wafer. This can occur via intraband absorption by free carriers – described by the fraction \( f_{\text{PR}} \) – or via band-to-band absorption which leads to photon recycling described by the fraction \( f_{\text{PR}} \). FCA within the wafer is insignificant for most practical cases of carrier densities below \( 10^{17} \text{ cm}^{-3} \) [21,51]. The fraction \( f_{\text{PR}} \) in a sample of thickness \( w \) with planar surfaces and no additional optical features affecting the in- or out-coupling of luminescence photons can be described reasonably well with the following term:

\[
 f_{\text{PR,planar}}(w, \Delta n) = 0.9835 + 0.006841 \log w(w) - 4.554 \times 10^{-9} \Delta n^{0.4612}
\]

(12)

(\( w \) given in cm, for range 0.0001 ... 0.1 cm; \( \Delta n \) given in \( \text{cm}^{-3} \) for \( \Delta n < 10^{17} \text{ cm}^{-3} \)).

The effect of total internal reflection will hence cause a strong reabsorption of emitted photons in planar samples. This case describes lifetime samples with passivated shiny-etched surfaces well and provides a good estimate for samples created from untextured silicon wafers. Since a pronounced surface texture or roughness greatly changes the angular distribution of photons after being reflected upon its first bounce, a smaller share \( f_{\text{PR}} \)
occurs for non-planar surfaces. Under the assumption that the surface texture of a sample creates a diffuse reflection the fraction

\[ f_{\text{diff}}(w) = 0.8681 - 0.044 \log_{10}(w) - 0.2393 \log_{10}(w)^2 - 0.117 \log_{10}(w)^3 \]

(w given in cm, in range 0.0001 \(\ldots\) 0.1 cm).

It should be kept in mind that these two given empirical terms describe cases with no or very good light trapping properties. Hence their usage should be accompanied by careful consideration whether a given sample should be approximated with these extreme cases.

References


[52] Andreas Fell simulations, Quokka 3.


