

Effect of Polymer Molecular Mass and Structure on the Mechanical Properties of Polymer–Glass Hybrids

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Cite This: *ACS Omega* 2022, 7, 786–792

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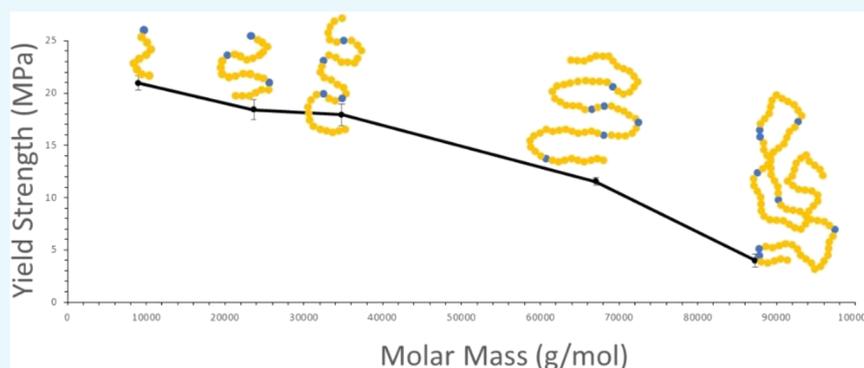
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ABSTRACT: Organic–inorganic hybrid materials are a promising class of materials for tissue engineering and other biomedical applications. In this systematic study, the effect of the polymer molecular mass (MM) with a linear architecture on hybrid mechanical properties is reported. Well-defined linear poly(methyl methacrylate-*co*-(3-(trimethoxysilyl)propyl methacrylate)) polymers with a range of MMs of 9 to 90 kDa and one 90 kDa star-shaped polymer were synthesized and then used to form glass–polymer hybrids. It was demonstrated that increasing linear polymer MM decreases the resultant hybrid mechanical strength. Furthermore, a star-polymer hybrid was synthesized as a comparison and demonstrated significantly different mechanical properties relative to its linear-polymer counterpart.

INTRODUCTION

Bone defects above a certain critical size, whether caused by trauma, bone tumor surgery, infection, or other causes, can have limited regeneration capability.¹ Currently, such defects are addressed using bone grafts, which involve disadvantages of the availability of patient's own bone and high invasiveness due to the requirement for multiple surgeries, bringing increased risk of infection.^{2,3} As such, biomaterial alternatives to grafting are of great interest.^{4–9} Inorganic–organic sol–gel hybrid materials are composed of inorganic and organic conetworks that are indistinguishable above the nanoscale and have been an active area of research with potential applications toward bone regeneration. Of particular interest are type II hybrids, which have covalent bonding between the organic and inorganic components, giving rise to a single-phase material with excellent mechanical properties.^{6–9} Some examples of such systems include polymer–clay hybrid nanocomposites,¹⁰ rubber–organomontmorillonite hybrid nanocomposites,¹¹ and polymer–silica hybrids.^{9,12}

In the context of bone regeneration, hybrids can overcome the brittleness of current inorganic synthetic bone grafts, such as bioactive glasses, which promote bone regeneration but cannot sustain cyclic loads and mitigate uneven degradation rates of the organic and inorganic components of conventional composites

of particles dispersed in a polymer matrix.^{9,13–17} Organic–inorganic sol–gel hybrids have previously been synthesized using polymers that contain pendant siloxane groups such as poly(3-(trimethoxysilyl)propyl methacrylate), polyTMSPMA. These polymers have been previously synthesized through a variety of polymerization methods such as reversible addition–fragmentation chain transfer polymerization, group transfer polymerization (GTP), and atom transfer radical polymerization.^{18–23}

In one of these studies, polymers of varying molecular masses (MMs) were fabricated, but the MM distributions were too broad to be able to correlate the mechanical properties of the hybrid with the polymer MM.¹⁸ In another interesting study, three polymers of different 3D topology were investigated, specifically branched *versus* star *versus* linear, and the resulting

Received: September 30, 2021

Accepted: December 14, 2021

Published: December 22, 2021



Table 1. Number Average Molecular Mass (M_n), Molecular Mass Distributions (\mathcal{D}) (See Supporting Information Figure S1 for the Gel-Permeation Chromatography (GPC) Traces), and Theoretical and Experimentally Determined Composition of All the Synthesized Copolymers

hybrid precursor polymer	polymer chemical structure	M_n (g/mol)	dispersity (\mathcal{D})	mol % TMSPMA	
				theo.	$^1\text{H-NMR}$
Linear-9 K	$\text{MMA}_{81}\text{-co-TMSPMA}_4$	8980 ^a	1.15 ^a	4	4
Linear-24 K	$\text{MMA}_{212}\text{-co-TMSPMA}_{10}$	23,600 ^a	1.11 ^a	4	5
Linear-35 K	$\text{MMA}_{313}\text{-co-TMSPMA}_{14}$	34,800 ^a	1.10 ^a	4	4
Linear-67 K	$\text{MMA}_{603}\text{-co-TMSPMA}_{27}$	67,100 ^a	1.13 ^a	4	4
Linear-87 K	$\text{MMA}_{785}\text{-co-TMSPMA}_{35}$	87,300 ^a	1.14 ^a	4	4
Star-90 K	$\text{MMA}_{806}\text{-co-TMSPMA}_{36}\text{-Star}$	89,700 ^b	1.21 ^b	4	4

^aDetermined using a GPC system with a refractive index (RI) detector, in THF, calibrated using poly(methyl methacrylate) standards.

^bDetermined using the RI detector within a triple detector GPC system.

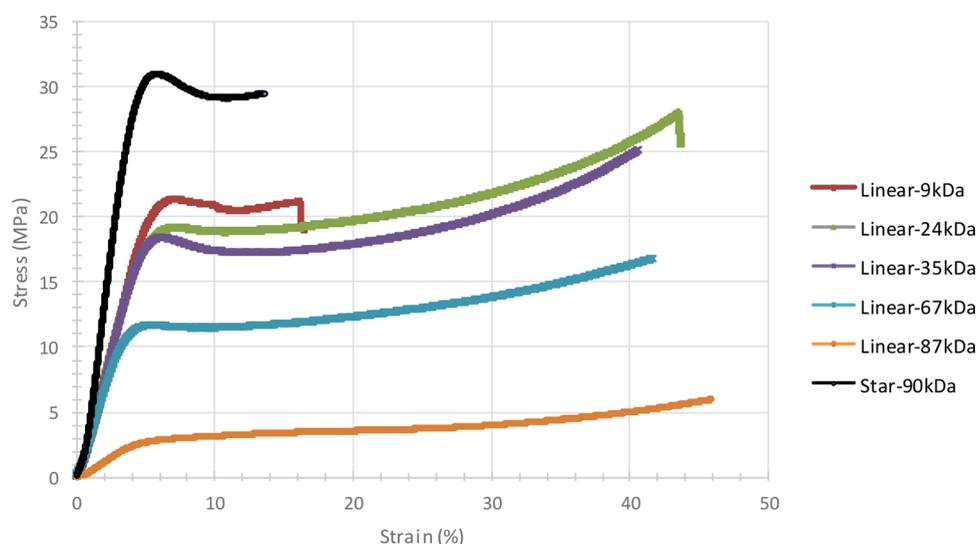


Figure 1. Characteristic stress–strain curves of hybrid materials made from different MM linear polymers and one star-polymer hybrid.

hybrids' mechanical properties varied significantly.²⁰ However, the MMs of the three polymers studied were not kept constant.

The aim of this study was to systematically investigate the effect of the linear polymer MM on glass/polymer hybrid mechanical properties through a comparative study of hybrid biomaterials produced from different MM linear polymers synthesized through one-pot GTP. A single set of hybrid samples produced from a star polymer with similar chemistry and MM to the largest linear polymer is also analyzed and compared. To the best of our knowledge, this is the first study where the MM effect is systematically investigated using polymers with narrow MMD as most published studies on TMSPMA-based polymers investigated polymers with broad MMD, no reported MMD, or they do not vary the MM.^{18–25} Thus, this work can serve as a guide for tailoring the mechanical properties of such systems in a variety of applications.

In this study, all copolymers of p(MMA-co-TMSPMA) were successfully synthesized via GTP with the targeted molar ratio of monomers, specifically ~4 mol % (~10 wt %) of TMSPMA (see Table 1), confirmed by proton nuclear magnetic resonance spectroscopy ($^1\text{H-NMR}$) (see Supporting Information Figure S2 for the nuclear magnetic resonance (NMR) spectra). This ratio was chosen because it was proven from previous studies that a high TMSPMA content results in brittle and easily faulted samples.¹⁸ See the Experimental Methods section at the bottom for details.

RESULTS AND DISCUSSION

To investigate the effects of polymer MM on the subsequent hybrid material's mechanical properties, five different MM linear copolymers were synthesized, while one star-shaped polymer was produced, using the same monomer units, monomer molar ratios, and with the same overall MM as the largest linear copolymer that was synthesized (90 kg/mol in total for the star-shaped polymer with ~9 kDa arms vs ~90 kDa linear copolymer). The polymers were synthesized through a similar process to previous studies involving GTP.^{26,27} In this case, for the statistical linear copolymers, the polymerization catalyst, solvent, and monomers were syringed into a round-bottom flask, and then the initiator was added to start the reaction. For the star-shaped copolymer, an arm-first one-pot synthesis approach was used where the same process as above was used to synthesize the linear copolymer arms, and then the still active linear polymers were then crosslinked using ethylene glycol dimethacrylate (EGDMA) as the crosslinking agent. The syntheses of all linear copolymers were terminated at 20 min, while the star-shaped polymer took a total of 40 min with 20 min for each stage. More details of the experimental procedure are provided after the conclusion.

Table 1 shows the number average MMs (M_n) and dispersity (\mathcal{D}) values of all the synthesized polymers. The M_n values for the linear copolymers ranged between 8980 and 87,300 Da to allow investigation of the effect of MM on the hybrids' properties. The

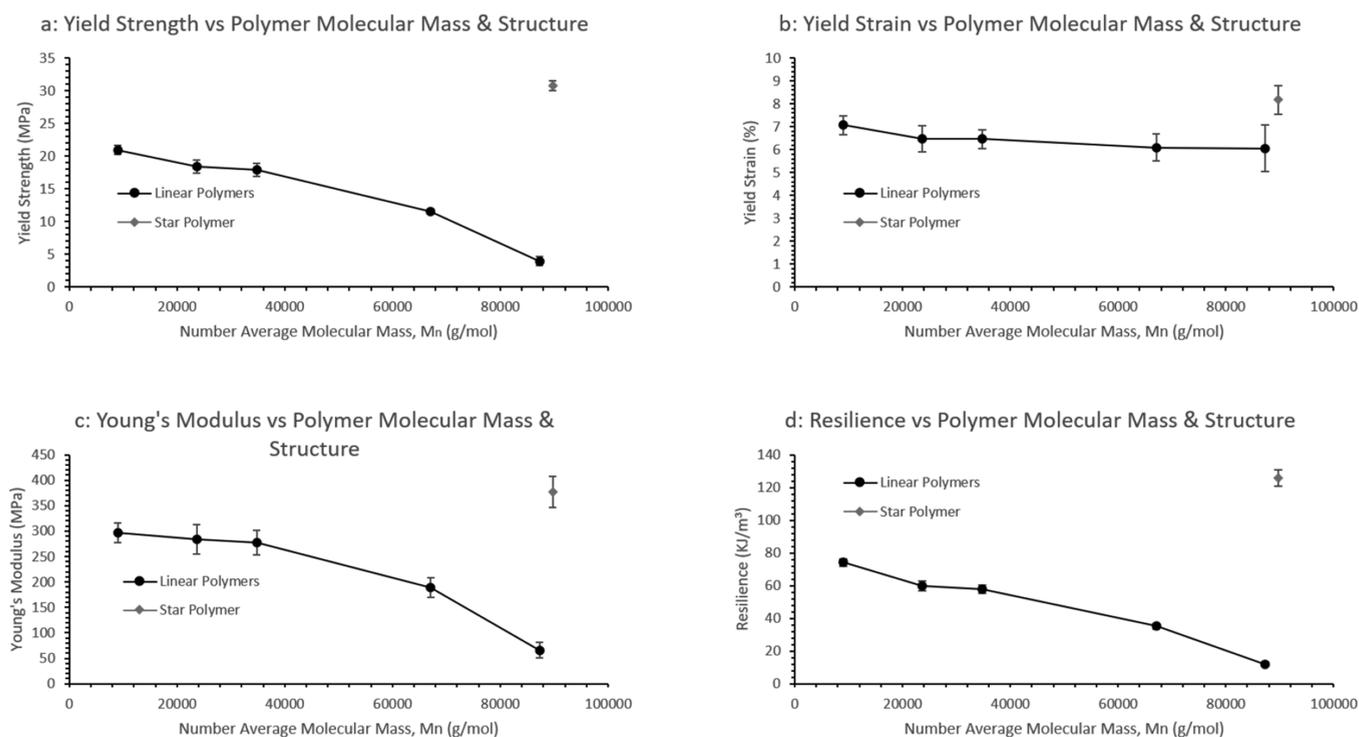


Figure 2. Hybrid mechanical properties as a function of MM for hybrids made with linear and star polymers: (a) Yield strength; (b) yield strain; (c) Young's Modulus; (d) resilience.

Table 2. Hybrid Compression Test and TGA Results

hybrid	yield strength (MPa)	yield strain (%)	resilience (kJ/m^2)	E (MPa)	residual mass (wt %)
Linear-9 K	21.0 \pm 0.70	7.06 \pm 0.39	74.1 \pm 2.4	297 \pm 19	15
Linear-24 K	18.4 \pm 0.95	6.48 \pm 0.57	59.7 \pm 3.0	284 \pm 29	10
Linear-35 K	17.9 \pm 1.0	6.46 \pm 0.42	57.9 \pm 2.5	277 \pm 24	12
Linear-67 K	11.5 \pm 0.36	6.09 \pm 0.59	35.1 \pm 1.8	189 \pm 19	14
Linear-87 K	4.00 \pm 0.63	6.06 \pm 1.0	12.1 \pm 1.4	66 \pm 15	17
Star-90 K	30.8 \pm 0.72	8.17 \pm 0.63	126 \pm 5.1	377 \pm 30	12

overall M_n of the star polymer is close to that of the highest M_n linear copolymer at 89,700 Da. The dispersity values were low, with \bar{D} less than 1.2 for the linear copolymers and just over 1.2 for the star-shaped polymers, indicating well-defined polymers. To the best of our knowledge, this is also the first time that GTP has been used to synthesize methacrylate-based linear copolymers of such high MM and low \bar{D} —with 2-(tigloyloxy)-ethyl methacrylate (TiEMA)-*b*-EGDMA at 67.8 kDa and a \bar{D} of 1.71 being one of the largest previously reported controlled GTP synthesized methacrylate copolymers.²⁷ The M_n values of the largest linear copolymer and of the star-shaped polymer were similar (<3% difference), enabling comparison between the mechanical properties of their hybrids.

All the synthesized copolymers were made into polymer–glass hybrid materials through the sol–gel process reported in previous studies.^{19–23} In brief, tetraethyl orthosilicate (TEOS) was used as the silicate source and was combined with water and hydrochloric acid (HCl) as a catalyst to undergo hydrolysis for 1 h. The synthesized polymer was then added to the reaction pot for polymerization with the hydrolyzed TEOS monomers. The resulting sol–gel was then poured into a screw top poly(methyl pentene) mold, then aged, and dried in an oven for 2 weeks for the hybrid to form and the solvents to evaporate, resulting in hybrids of approximately 15 mm length and 8 mm in diameter.

Six samples of cylindrical shaped hybrids suitable for uniaxial compression tests were produced for each different polymer (See Supporting Information Figure S4 for sample pictures). These were then compression tested according to the ISO 604:2003 standard for plastics compression tests where samples were tested at 5 mm/min without preloading. Thermogravimetric analysis (TGA) was used to characterize their organic to inorganic compositions (see Supporting Information Figure S3). The synthesized hybrids all had similar residual mass (silica glass) after thermal degradation at around 15 wt %, which was similar to the nominal composition.

All the different hybrids had clear elastic deformation and plastic deformation regimes that facilitated yield point identification (Figure 1). Hybrids synthesized from polymers of different MMs performed differently during uniaxial compression tests. The key finding here is that as the MM for the linear copolymers increased, yield strength of the hybrids decreased (Figure 2). Hybrids made from the 9 kDa M_n linear copolymers averaged 21 MPa in yield strength (Table 2), whereas the hybrids made from 87 kDa M_n linear copolymers only averaged 4 MPa in yield strength. The decrease in yield strength with increasing linear copolymer M_n is consistent and clearly observed and has low error. The strain behavior was similar for all the hybrids synthesized from different M_n at 6 to 7% strain. As a result, Young's moduli and resilience (area under

Aldrich, United Kingdom. Tetrabutyl ammonium bibenzoic acid (TBABB) was synthesized previously in the lab and used as is.

Linear-Polymer Synthesis through GTP. First, all monomers were purified through two columns of basic alumina, while TMSPMA was passed through one column of neutral alumina. After purification, the monomers were placed in round-bottom flasks where calcium hydride (CaH_2) was added. Additionally, DPPH was added to all purified monomers as an inhibitor. The round-bottom flasks were then sealed with a stirrer bar, a rubber septum each, and wrapped with parafilm. The purified monomers were then placed in a fridge for CaH_2 to absorb any residual moisture for a minimum of 72 h before the next steps. MTS was used as is from the manufacturer, taken directly from the fridge when needed.

After sufficient drying with CaH_2 , the monomers were distilled via vacuum distillation. Upon distillation, the Schlenk tubes were then purged with argon gas, sealed with rubber septa, wrapped with parafilm, and placed in the fridge to await polymerization.

Syntheses of the linear block copolymers were carried out through GTP (Figure 4). As an example, the synthesis of the

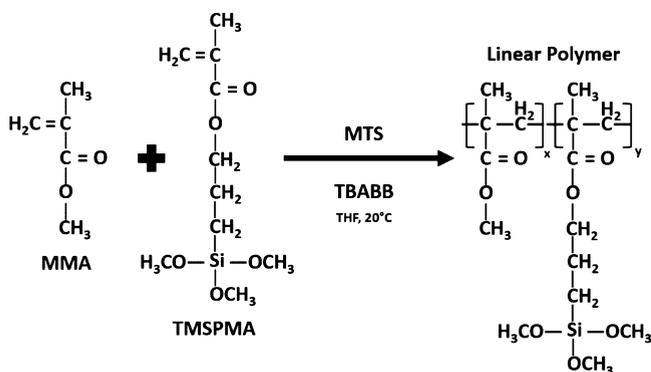


Figure 4. GTP of MMA-co-TMSPMA copolymers from monomers.

targeted 8 kDa, 90 wt % MMA – 10 wt % TMSPMA linear polymer is provided in brief: 10 mg of TBABB catalyst was added into a 250 mL round-bottom flask which was then sealed with a rubber septum. Argon was used to purge and displace the air in the flask to eliminate moisture. THF polymer solvent (47.99 mL) was then syringed into the sealed flask. Then, 12.06 mL of MMA monomer (0.113 mol, 11.34 g) and 1.21 mL of

TMSPMA monomer (0.005 mol, 1.26 g) were syringed into the flask. The MTS initiator (0.32 mL) was quickly syringed into the sealed flask and temperature began to increase, indicating a reaction. The temperature increased from 23.8 to 40.6 °C and stopped increasing which indicated the termination of the polymerization. Two 1 mL samples of the polymer were extracted using a syringe and placed in two separate small glass vials for later use in GPC and $^1\text{H-NMR}$ spectroscopy. At the 20 min mark since the start of polymerization, two drops of methanol were added to both sample vials, and 1 mL of THF solvent was added to the GPC sample vial. Both samples in the vials were then thoroughly mixed using fresh disposable syringes. All linear polymers were synthesized in the same fashion but with different amounts of reagents.

Star-Polymer Synthesis Arm-First Approach through GTP. Star-polymer synthesis is carried out in an arm-first fashion where linear polymer arms were synthesized using the same method as outlined in the previous section (Figure 5). To form the star polymers, 1.49 mL of EGDMA crosslinker (0.008 mol, 1.56 g) was syringed into the sealed flask with active 8 kDa linear polymers, and the temperature increased from 25.6 to 27.7 indicating the start and end of the crosslinking reaction. At the 20 min mark since the start of polymerization the reaction was terminated with methanol, two star-polymer samples were collected in the same fashion as previously for GPC and $^1\text{H-NMR}$.

Star-Polymer and Linear-Polymer Purification. To purify polymers, large glass beakers (800 mL+) were filled with four parts ethanol and one part hexane with a stirrer bar added. These were placed on their respective stirrer plates. Aluminum foil was used to cover each beaker, two holes were then punctured, and then using a needle connected to the argon line, the beaker was filled with argon gas for 3 min. While the hexane-ethanol solution was stirred, the polymers to be purified were poured into the prepared beakers directly from their respective round-bottom flasks while dissolved in THF. Once polymers visibly precipitate to the bottom of the beakers, the liquid content of the beakers was carefully poured out into a spare beaker until only the precipitated polymers remain in the beakers. These were then redissolved in THF, filled with argon gas, and sealed with aluminum foil. Upon fully dissolving, GPC samples were taken with the same steps as sample collection during polymerization. The GPC samples are analyzed to see if any undesirable peaks remained. The purification process was repeated until as much of the undesired peak was removed as

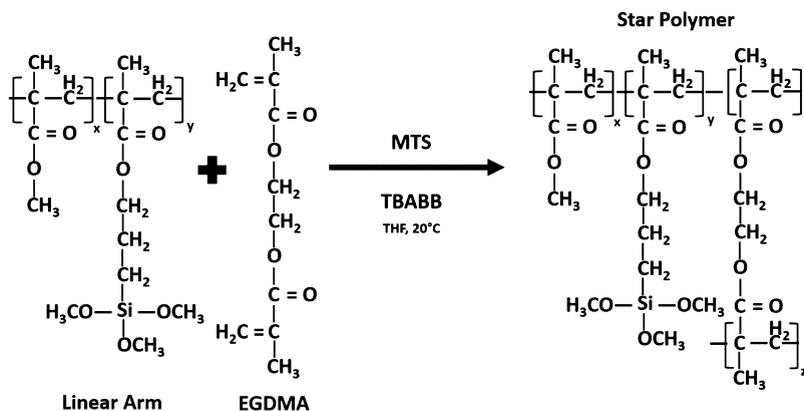


Figure 5. GTP of MMA-co-TMSPMA-star star polymers from the linear arm and EGDMA.

possible, the process was stopped when additional purification resulted in no difference in polymer peaks.

Gel-Permeation Chromatography. First the samples previously taken during polymer syntheses were filtered by syringing them through Millex-LCR filters. The GPC solvent used was pure HPLC-grade THF calibrated using prefabricated reference poly(methyl methacrylate) samples of 2000, 4000, 8000, 20,000, 50,000, and 100,000 Da. These were calibrated on a SECurity GPC system with the Polymer Standards Service SDV analytical M column (SDA083005LM). Both linear polymers and star polymers were analyzed with a RI detector. For star polymers, additional analysis was performed through triple detection using combined RI, light scattering, and viscometry. For star polymers, additional analyses on polymer branching were performed by plotting a Mark–Houwink plot of molecular weight vs intrinsic viscosity to confirm branching and formation of star polymers.

Hybrid Synthesis through the Sol–Gel Process. Syntheses of the organic–inorganic hybrid materials were carried out through the sol–gel process. A representative procedure for a 90 wt % organic content hybrid is outlined here. First, hydrolysis of TEOS was started by the addition of 2.989 mL TEOS, 0.965 mL deionized water, and 0.322 mL of 1 M HCl into a polytetrafluoroethylene (PTFE) stirring container in a molar ratio of 1:4:0.00016 respectively (water to HCl is a volume ratio of 4 to 1). A stirrer bar was added, the container sealed, then the solution was left to react for an hour to fully hydrolyze. While the TEOS was undergoing hydrolysis, dissolved polymer containing 9.25 g of the polymer was put under a rotary evaporator until fully dry, then immediately dissolved in THF at a concentration of 1 g/mL. Once the TEOS fully hydrolyzed, the prepared polymer was poured into the TEOS container then resealed. The reaction was allowed to proceed for up to 3 min, and then the sol–gel was poured into prepared PTFE molds and then placed in a PTFE container with a lid. The container with the mold was then sealed and placed in a 40 degrees Celsius oven to age. The aging process took 2 weeks.

Proton Nuclear Magnetic Resonance Spectroscopy. ^1H -NMR spectroscopy was used to confirm the composition of polymers using deuterated chloroform and a 400 MHz Avance Bruker NMR spectrometer. Samples were prepared by dissolving 0.1 mL of a sample polymer in up to 2 mL of CDCl_3 , mixed well with a pipette, and then deposited in an NMR tube.

Hybrid Mechanical Tests. Mechanical properties of hybrid materials were evaluated via uniaxial compression tests conforming to the ISO 604:2003 standard for plastics compression tests. Cylindrical hybrid specimens where the height/diameter ratio is greater than 1 were synthesized for compression tests. Sanding paper was used to manually grind the specimen ends to flat and parallel states. A caliper was used to measure the height and cross-sectional width of the specimen at different orientations 5 times and then used to obtain average values for both dimensions. A Zwick 1474 instrument with a compression speed of 0.5 mm/min and 10kN load cell was used for testing. The raw data obtained consisted of force applied over compression plate moving distance. These values were then used to calculate engineering stress and strain using the following formula:

$$\text{Stress, } \sigma = \frac{F}{h\pi r^2}$$

$$\text{Strain, } \varepsilon = \frac{\Delta h}{h}$$

Where F is the force in newtons, h is the sample height in mm, r is the sample radius, and Δh is the compression plate movement distance in mm. Resilience was found as area under the stress–strain curve up to the end of the linear region.

Thermogravimetric Analysis. A NETZSCH STA 449C TGA machine was used to measure the organic content of hybrid material samples. Hybrid samples were ground to a fine powder manually using a crucible and grinder. Between 10 and 30 mg of powder were placed in platinum crucible cleaned with acetone and with prior measured mass. The samples were then heated up to 800 °C at 10 °C/min with continuously supplied air to burn away organic components. The mass change over temperature is plotted, and the inorganic content was determined by the leftover mass at the end of the measurement.

■ ASSOCIATED CONTENT

Supporting Information

The Supporting Information is available free of charge at <https://pubs.acs.org/doi/10.1021/acsomega.1c05424>.

Materials, experimental procedures, GPC spectra, ^1H NMR spectra, and compression test stress–strain curves (PDF)

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Author Contributions

The manuscript was written through contributions of all authors. All authors have given approval to the final version of the manuscript.

Notes

The authors declare no competing financial interest.

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