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# The fragility of thermoelectric power factor in cross-plane superlattices in the presence of non-idealities: A quantum transport simulation approach

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## Abstract

Energy filtering has been put forth as a promising method for achieving large thermoelectric power factors in thermoelectric materials through Seebeck coefficient improvements. Materials with embedded potential barriers, such as cross-plane superlattices provide energy filtering, in addition to low thermal conductivities, and could potentially achieve high figures of merit. Although there exist many theoretical works demonstrating Seebeck coefficient and power factor gains in idealized structures, experimental support has been scant. In most cases the electrical conductivity is drastically reduced due to the presence of barriers. In this work, using quantum mechanical simulations based on the Non-Equilibrium Green's Function method, we show that although power factor improvements can theoretically be observed in

optimized superlattices (something pointed out in previous studies), different types of deviations from the ideal potential profiles of the barriers degrade the performance. Some non-idealities being so significant as to negate all power factor gains. Specifically, the effect of tunneling due to thin barriers could be especially detrimental to the Seebeck coefficient and the power factor. Our results could partially explain why significant power factor improvements in superlattices and other energy filtering nanostructures mainly fail to be realized, despite theoretical predictions.

*Index terms:* thermoelectric, superlattices, quantum transport, thermoelectric power factor, Seebeck coefficient, energy filtering

## I. Introduction

The thermoelectric (TE) performance of materials is determined by the figure of merit  $ZT = \sigma S^2 / \kappa$ , where  $\sigma$  denotes the electrical conductivity,  $S$  the Seebeck coefficient and  $\kappa$  the thermal conductivity. Large improvements in  $ZT$  have recently been reported in nanoscale materials due to drastic reduction in  $\kappa$  [1, 2]. On the other hand, efforts to improve the power factor ( $\sigma S^2$ ) have met with less success, and overall  $ZT$  still remains low. Energy filtering in nanocomposite materials with embedded potential barriers (of height  $V_B$ ) is a promising way to improve  $\sigma S^2$  via improvements of the Seebeck coefficient [2-18]. Cross-plane superlattices are some of the first structures considered in order to utilize energy filtering [3,6,7,9]. In these structures, although the theoretical expectation of power factors gains is high  $\sim 40\%$  [5,10,11,15], the accompanying experimental verification has been lacking, with the exception of the work of Ref. [7]. Regarding power factor gains, experimental demonstration, to the best of our knowledge, is completely lacking. The work of Ref. [12,16] has demonstrated very high power factors in Si-based nanocomposites, however energy filtering was only partially responsible for this. Surprisingly, despite the fact that the energy filtering idea was suggested in the 1998 [5], still there is no theoretical investigation as to why power factor benefits are hard to realize experimentally.

In this work, we use the Non-Equilibrium Green's Function (NEGF) method to demonstrate that, although  $\sigma S^2$  can be theoretically improved within an optimized geometry, different types of variation from the idealized shape act as strong detrimental



$$\Sigma^{\text{in/out}} = \Sigma_{\text{scatt}}^{\text{in/out}} + \Sigma_1^{\text{in/out}} + \Sigma_2^{\text{in/out}} . \quad (3)$$

In these equations,  $H$  is the Hamiltonian of the channel of interest,  $i\eta$  is an imaginary infinitesimal and  $\Sigma_{1,2}$  and  $\Sigma_{\text{scatt}}$  are the perturbative self-energies capturing the effect of the left and right contacts and the scattering processes (acoustic and optical phonon scattering), respectively. The corresponding  $\Sigma_{1,2}^{\text{in/out}}$  is defined as  $\Sigma_{1,2}$  times the Fermi-Dirac distribution for “in” or one minus the Fermi-Dirac distribution for “out” and  $\Sigma_{\text{scatt}}^{\text{in/out}}$  is defined below. The scattering self-energies are taken here to have only two components resulting from optical ( $\Sigma_{\text{OP}}$ ) and acoustic ( $\Sigma_{\text{AP}}$ ) phonon scattering. As is common practice, the self-energies of phonon scattering are taken to be diagonal in the real space basis (amounting to the assumption that phonon scattering is local) and acoustic phonon collisions were assumed to be elastic and optical phonons assumed to have a flat bandstructure. Thus, the self-energies of optical phonons are taken to be:

$$\Sigma_{\text{OP}}^{\text{in}}(E) = D_{\text{OP}\omega}(n+1)G^n(E+\hbar\omega) + D_{\text{OP}\omega}nG^n(E-\hbar\omega) \quad (4a)$$

$$\Sigma_{\text{OP}}^{\text{out}}(E) = D_{\text{OP}\omega}(n+1)G^p(E-\hbar\omega) + D_{\text{OP}\omega}nG^p(E+\hbar\omega) \quad (4b)$$

and those of acoustic phonons taken to be

$$\Sigma_{\text{AP}}^{\text{in/out}} = D_{\text{AP}}G^{n/p}(E) . \quad (5)$$

In this formalism, we assume deformation potential scattering, where the strength of electron-phonon scattering by phonons in the self energies  $\Sigma^{\text{in/out}}$ , is captured by the constants  $D_{\text{AP}}$  and  $D_{\text{O}}$  that describe acoustic and optical phonons, which is common practice in electronic transport calculations. We do not compute the phonon spectrum, despite the fact that in a superlattice geometry it could be different compared to bulk. We

still use this common approximation as the focus of the work is on electronic transport, and not on the phonon details, or heat transport.

An effective mass model was used with a value of  $m_{\text{eff}} = 1.0m_e$  ( $m_e$  being the mass of a free electron) and a lattice spacing of  $a_0 = 0.5\text{nm}$ . The energy of the optical phonons ( $\hbar\omega$ ) was chosen to be  $60\text{meV}$  and the values of the acoustic and optical phonon couplings strengths were taken to be equal (i.e.  $D_{AP} = D_{OP} = D_0$ ), this was done to minimize the number of tunable parameters in the system. The value of  $D_0$  was chosen in a manner discussed below. For further information on the NEGF method the reader is referred to the book of Datta [19] which is entirely dedicated to a pedagogical introduction to the method.

The power factor,  $GS^2$ , is calculated from the expression

$$I = G\Delta V + SG\Delta T. \quad (6)$$

For each value of the power factor, the calculation is done twice, initially with a small potential difference and no temperature difference ( $\Delta T=0$ ) yielding the conductance ( $G = I_{(\Delta T=0)}/\Delta V$ ), then again with a small temperature difference and no potential difference ( $\Delta V=0$ ) yielding the Seebeck coefficient ( $S = I_{(\Delta V=0)}/G\Delta T$ ). This method was validated in Ref. [10]. Convergence of the self-consistent scattering was measured through the requirement of current conservation throughout the system. A convergence value of 5% conservation was chosen (i.e. convergence is reached if the current varies by no more than 5% along the length of the channel). The sharp features of the system required a very large number ( $\sim 1000\text{s}$ ) of convergence steps. A 100 different device structures were simulated overall in order to gather enough data for the effect of non-idealities on the

power factor of superlattices. Only the imaginary part of the scattering self-energy included. The relevant matrix problems were solved using the recursive Green's function (RGF) method [20].

Figure 1 illustrates the simulated 1D channel geometry. Figure 1a shows the channel as a series of potential barriers, which is the base geometry we consider, Fig. 1b shows the extracted local density of states  $LDOS(E,x)$  from NEGF, Fig. 1c the charge density in the channel. Note the charge fluctuations in space and energy, formed by quantum interference. Figure 1d the current spectrum and how it fluctuates in energy during emission / absorption of optical phonons. The red line above the barriers indicates the average current spectrum energy. This first check indicates that the simulator functions properly as required.

The next step is to calibrate the basis geometry to initially provide optimal power factor values from which a study of detrimental effects can be undertaken. Previous works have indicated that under optimal conditions the power factor can be improved by up to  $\sim 40\%$ , compared to the pristine material with a flat potential [5,10,11,15]. For this to be achieved, however, the transport in the wells needs to be semi-ballistic, where carriers only lose part of their energy before they reach the next barrier [6, 11]. In addition, it was also indicated that ideally the barrier height needs to extend  $\sim k_B T$  above the Fermi level [6]. Finally, the Fermi level needs to be placed high enough in energy to provide carriers with high velocities and conductivity. Thus, in this work we calibrate the geometry, electron-phonon scattering, Fermi level, and barrier height for these optimal

conditions and use the calibrated geometry as a base, before we start to consider the influence of non-idealities in the design parameters. The calibration procedure is as follows: i) A channel of length  $L_{\text{ch}}=20\text{nm}$  is considered with flat potential across it. ii) The position of the Fermi level  $E_F$  for maximum ballistic conductance  $G$  is identified. The conductance  $G$  versus  $E_F$  is shown in Fig. 2a. The position of  $E_F$  for maximum  $G$  is indicated by the blue-dashed line. This is observed at  $E_F=0.14\text{eV}$ . iii) Using that channel and Fermi level, the electron-phonon scattering interaction is increased (i.e. deviate from the ballistic case towards diffusive transport) until the conductance drops to 50% of the ballistic limit (achieving 50% ballisticity in the channel). The value of the electron-phonon interaction used for this is  $D_0=0.0016\text{ eV}^2$  (see Ref. [21] for the details of the formalism and how  $D_0$  is used). Figure 2b shows how the conductance changes in the 20nm channel versus  $D_0$ , and the 50% ballisticity value is indicated by the red-dashed line.

### III. Results and Discussion

Once the calibration is completed, we proceeded by forming the superlattice geometry and then by investigating the performance of energy filtering processes under unintended variations in the design parameters away from the optimal case, that could be the usual case in experiments. To form the structure geometry we place a series of wells and barriers as in Fig. 1a, with the length of the wells being 20nm and the width of the barriers being 4nm, and the Fermi level  $E_F$  is placed at  $E_F=0.14\text{eV}$ .

The first parameter we examine is the shape of the barriers/wells. In practice, an ideal rectangular barrier might not be achievable, thus we examine the influence of deviations from the rectangular shape on the performance. In this case, we model the shape of barrier as a Gaussian function (see inset of Fig. 3), and we vary the variance. For small variances, the barriers will approach a delta-function potential, whereas large variances will tend to recover very thick barriers with a limiting case of a single barrier structure. Crucially, we denote this limiting single barrier structure as a “bulk thermoelectric structure” and take it as a comparison case. Should power factor performance be worse than this case, then the superlattice structure is offering no enhancement. Thus, power factor values below this point, marked by a dotted magenta line in the figures to follow, represents a loss of all power factor gains from the superlattice structure. Figure 3 shows the power factor versus the Gaussian distribution variance (the shapes of the distributions are also shown in the inset). Structures with different barrier heights, from  $V_B=0.14\text{eV}$  to  $V_B=0.18\text{ eV}$  are indicated. Although the barrier heights do not have significant qualitative influence on the power factor, the variance can have a strong influence. In the left side of Fig. 3, for delta-shape potentials, the power factor is significantly lower as a result of increasing quantum mechanical tunneling from the barriers, which significantly degrades the Seebeck coefficient. At the right side of Fig. 3, on the other hand, the power factor approaches that of the pristine, flat potential material (magenta-dashed line) as expected, since the barriers get significantly thicker with variance. In the middle region, however, an improvement of the power factor is observed for variances around  $0.7\text{ nm}^2$ , resulting in a power factor value

similar to the optimal one achieved by square barriers (see Fig. 5 below). Thus these results indicate that the shape of the barriers is important, and care needs to be taken in their design, especially in avoiding the possibility of tunneling.

To further stress the detrimental effect of quantum mechanical tunneling from thin barriers, the left axis of Fig.4 (black) shows the power factor versus barrier width for the starting geometry with perfect square shaped barriers. Indeed, similarly to Fig. 3, in the left side, thin barriers allow significant tunneling, which degrades the Seebeck coefficient and diminishes the power factor. As the width increases, the power factor increases, but then for larger widths the power factor begins to slightly drop again, in the limit of infinite barrier width it approaches the single barrier flat potential channel. The reason is that the channel resistance increases with barrier width as the carriers relax near the bottom of the barrier conduction band more effectively. Carrier velocities and conductivity at those energy regions are low. The less barrier space in the channel, the better for the conductivity, but large amount of tunneling should be avoided. An optimal point can be found in the middle region for barrier widths of  $W=3\text{nm}$ , which is thick enough to prevent sufficient tunneling to erode the energy filtering effect, but thin enough to prevent resistance increase. To further demonstrate that the power factor loss for ultra-thin barriers is due to an increase in tunnelling, and that the amount of tunneling for barriers above  $W=3\text{nm}$  is not sufficient to further erode the power factor, the right axis of Fig. 4 (blue), shows the ratio of the current contribution from tunneling to the total current. Indeed, tunneling decreases monotonically, contributing only  $\sim 35\%$  at  $W=3\text{nm}$ . This can be quite significant, but its effect on the power factor is limited. It is also clear

that the sudden drop in power factor for  $W < 2\text{nm}$ , going even below the magenta line, coincides with the increase in the fraction of the total current tunneling through the barriers.

The final non-ideality we examine is the effect of the well shape alone. The motivation for this, is to isolate the effect of the barrier shape and the well shape, in order to better understand the non-idealities in the shape of the well. For this, we consider a flat top rectangular barrier with fixed thickness, but allow for a decay of the potential into the well with a decay length  $\xi$  as shown in the insets of Fig. 5a and 5b. The rectangular barriers are ideal (left side limit of  $\xi=0$ ), which shows that  $\sim 30\%$  improvement can be achieved compared to the bulk TE material case with flat potential (magenta-dashed line). As we deviate from that shape the power factor drops (approaching the bulk case – right side). For this to happen, however, significant distortion needs to be applied to the shape of the well (compare right inset to left inset in Fig. 5).

## IV. Conclusion

Using the NEGF method we computed the thermoelectric power factor in nanocomposite channels in the presence of energy barriers designed to enhance filtering, and, thus, thermoelectric power factors. While ideally, as has been known in previous works [5,10,11,15], power factor improvements up to 30% can be achieved using energy filtering under optimal conditions, we show that this improvement is sensitive to structural imperfections. Fluctuations in the barrier width, barrier shape, and well shape,

could degrade the performance significantly and could take away most of the power factor improvements provided by the superlattice geometry. Especially, barriers with width or shape that allows significant quantum mechanical tunneling cause large degradation to the power factor. Our results indicate that superlattice thermoelectric material designs should be fabricated close to ideal geometries if benefits are to be provided, which might be an indication as to why to-date significant power factor benefits were not observed by energy filtering.

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Figure 1:

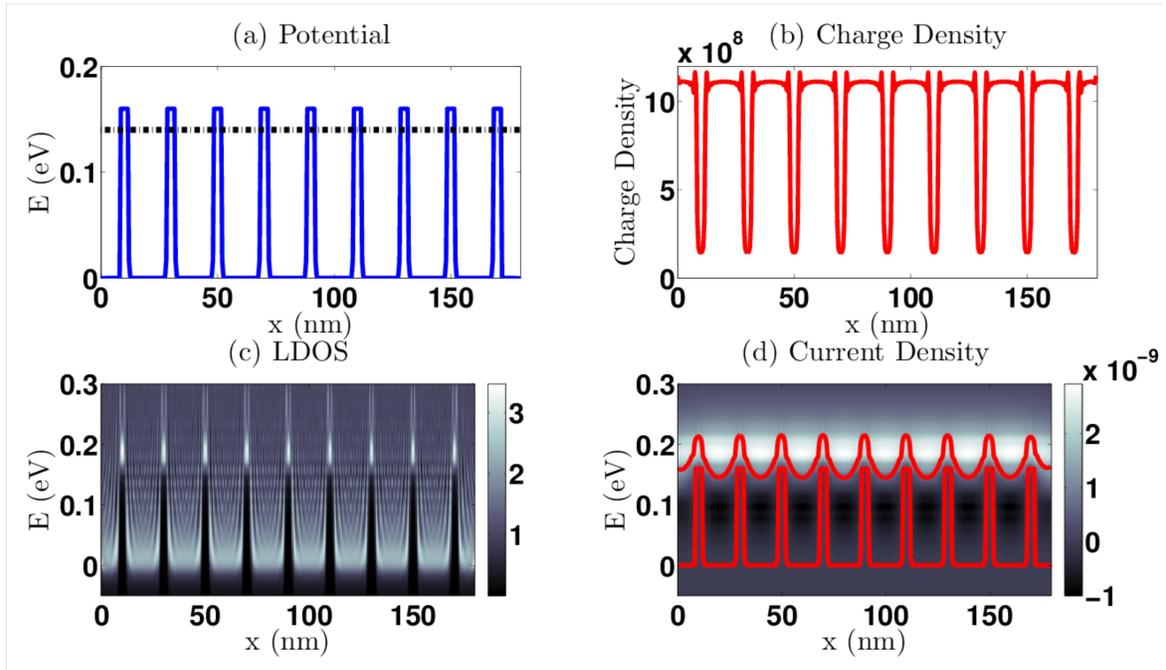


Figure 1 caption:

Sample data for a nanocomposite channel. (a) The potential profile of the barriers in the channel with width of 4nm and height of 0.16 eV. (b) The local density of states in the channel. (c) The charge density. (d) The current density versus position (colormap). Superimposed on the image are the potential barriers and the carriers energy expectation value  $\langle E \rangle$ .

Figure 2:

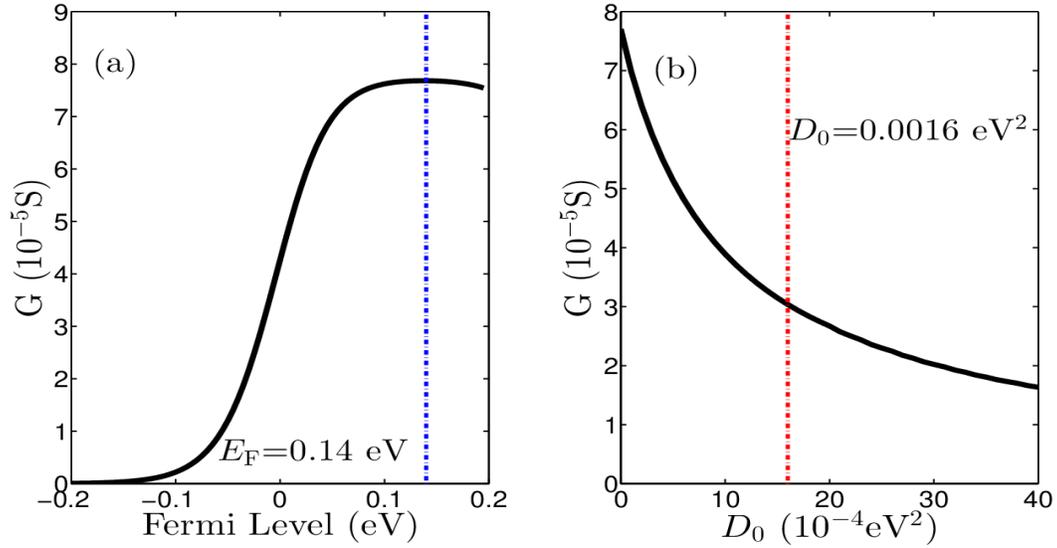


Figure 2 caption:

The calibration of the model and initial channel material. A channel of length  $L_{\text{ch}}=20\text{nm}$  is used. (a) The position of the Fermi level for maximum ballistic conductance  $G$  is identified. The maximum, conductance is observed for  $E_F=0.14\text{eV}$ . (b) Using that channel and Fermi level, the electron-phonon interaction is increased until the conductance drops to 50% of the ballistic limit (achieving 50% ballisticity).

Figure 3:

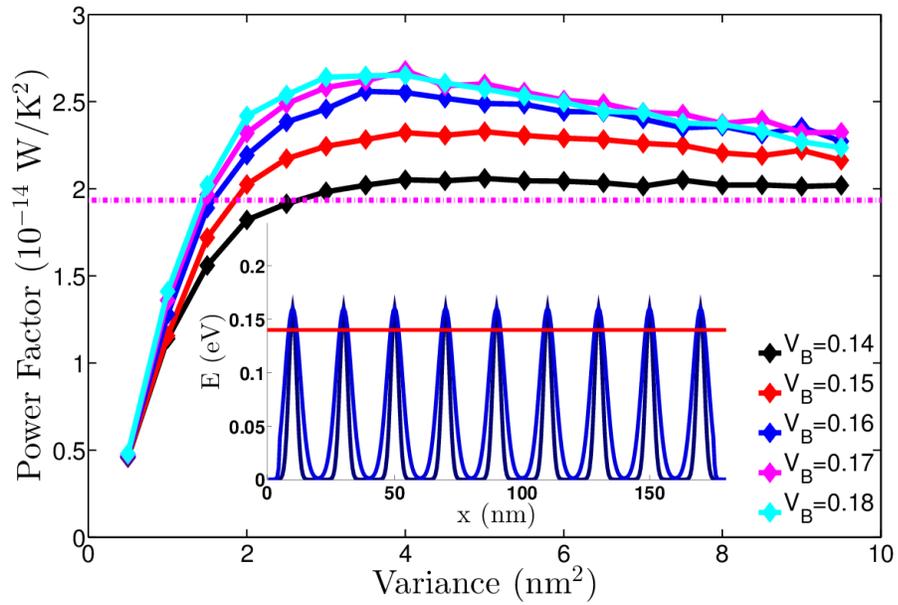


Figure 3 caption:

The power factor of a superlattice material geometry upon deviations of the shape of the barrier/wells from a square into a Gaussian-like shape. Materials with different barrier heights, from  $V_B=0.14\text{eV}$  to  $0.18\text{eV}$  are shown. Inset: The potential profiles in channels with Gaussian shaped barriers and wells.

Figure 4:

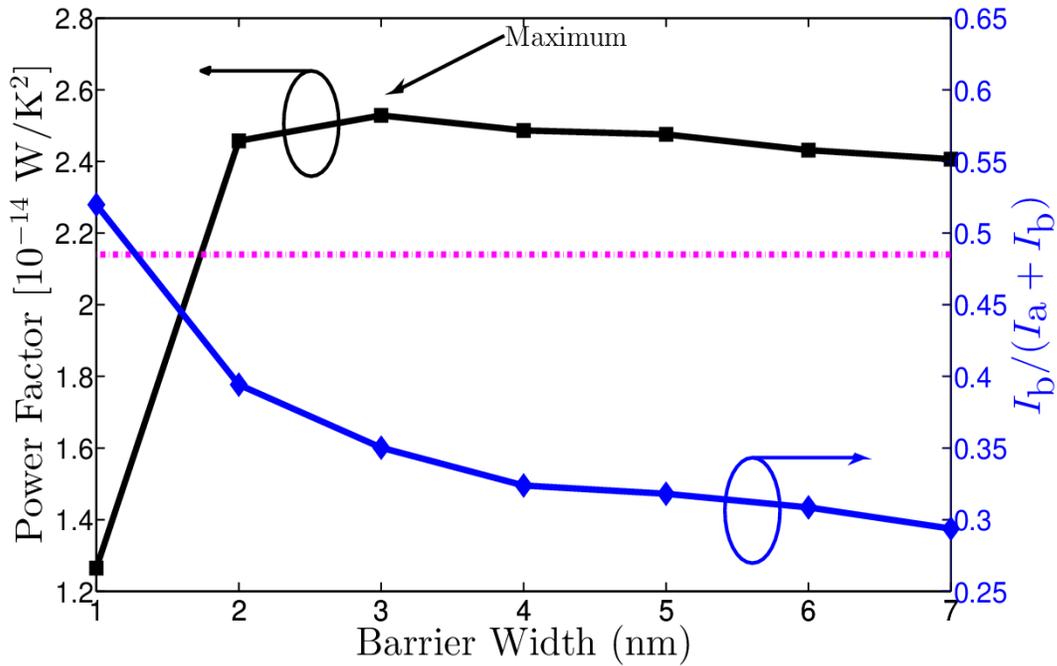


Figure 4 caption:

Left axis (black): Power factor versus barrier width. The optimal barrier width is ~3nm, which is thick enough to prevent large amount of tunnelling, but thin enough to keep the electrical resistance from barriers low. At very thin barriers (< 3nm) power factor drops rapidly becoming worse than the bulk thermoelectric case (magenta line). Right axis (blue): The fraction of the current that is contributed by tunneling  $I_b$  (i.e. flows below the barriers) compared to the total current, flowing above and below the barriers,  $I_a+I_b$ . It is clear that the dramatic loss in power factor for ultra-thin barrier widths coincides with the increase in tunneling current through the barriers.

Figure 5:

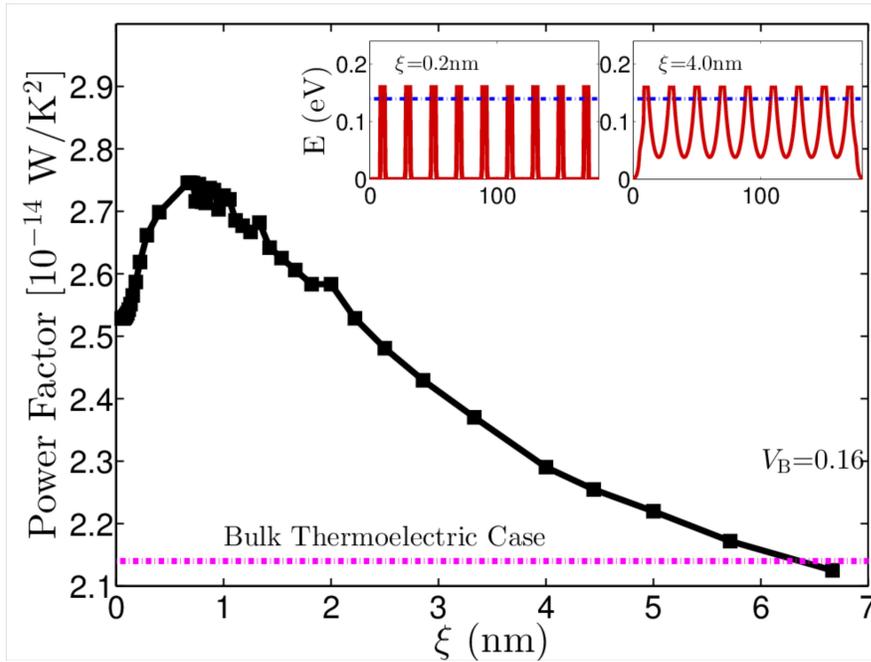


Figure 5 caption:

Power factor versus barrier shape, defined as an exponentially decaying profile, described by a decay length,  $\xi$ , from the top of the barrier. The limit  $\xi=0$  corresponds to a square barrier (left side), which is found to be the optimal one. Insets: Potential profiles in the superlattice structure under different values of  $\xi$ .