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Modified S² schemes for estimating differential mode group delay in polarization-maintaining few-mode fiber

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Abstract: In the mode-division-multiplexed (MDM) system, the few-mode fiber (FMF) replaces the single-mode fiber (SMF) as the 8 transmission medium, to increase the per-fiber transmission capacity. The polarization-maintaining few-mode fiber (PM-FMF) can 9 greatly enhance the optical communication system, since it can both preserve the polarization state and allow the transmission of 10 multiple modes. To obtain the differential mode group delay (DMGD) value of the PM-FMF, which determines the computational 11 complexity of the equalization algorithm at the receiver, the characterization of the fiber is essential. The conventional S² method, 12 which can estimate the DMGD of the FMF, cannot be directly applied to the PM-FMF, because the dominant mode of the PM-FMF 13 fiber cannot be determined. In this work, two new approaches are developed, for the first time to our knowledge, to measure the 14 DMGD in the PM-FMF. The former method is to measure the DMGD in both polarization directions, and LP_{01x} and LP_{01y} are selected 15 as dominant modes, respectively. The latter approach is to realize a simultaneous DMGD measurement of all LP modes, and only 16 LPoily is selected as the dominant mode. It is demonstrated in the experiments that a good agreement has been achieved between the 17 measurement results from both schemes. 18

Keywords: differential mode group delay; polarization-maintaining few-mode fiber; spatially and spectrally resolved imaging; optical communication system

1. Introduction

Mode-division-multiplexed (MDM) systems using few-mode fibers (FMFs) have recently received much attention 23 because of their potential to increase the per-fiber transmission capacity [1,2]. In the MDM system, each mode carries 24 independent information, and in an ideal FMF, the modes propagate without any crosstalk [3]. However, in the practical 25 optical fiber, the distribution of the refractive index may vary along the direction of propagation (due to the fiber draw-26 ing or macro-/micro-bending). In order to obtain the actual differential mode group delay (DMGD) value of the FMF 27 which determines the number of required taps in the equalization algorithm at the receiver, the characterization of the 28 fiber is essential. Since the computational complexity of the equalization algorithm scales with the total DMGD of the 29 fiber [4], it is necessary to design a fiber with a low DMGD. This also requires the characterization of the actually pro-30 duced fiber. A typical characterization method is spatially and spectrally resolved imaging (S²), where the characteristic 31 parameter of the DMGD is extracted according to the beat frequency generated between each mode [5,6]. Using this 32 method, the DMGD and the mode field information of the FMF can be measured accurately [7-9]. The polarization-33 maintaining fiber (PMF) is one branch of special optical fibers which can maintain the state of the polarization [10]. The 34 polarization-maintaining few-mode fiber (PM-FMF), combining the characteristics of both PMF and FMF, has been 35 demonstrated to achieve the MIMO-free polarization- and mode-multiplexed transmission [11]. Moreover, PM-FMFs 36 are also widely used in the field of fiber sensing, which can realize the simultaneous sensing of multiple parameters 37 [12]. In 2019, Liu et al. proposed a modified method for simultaneously measuring the beat length of all guided modes 38 in a PM-FMF [13], but it is still a difficult problem to realize the simultaneous measurement of the DMGD between all 39 LP modes in PM-FMFs accurately and effectively. Traditional S² method cannot be directly applied in the measurement 40 of PM-FMF, because it is impossible to determine the dominant mode of PM-FMF, and the conventional interference 41 equation of S² is not applicable to the PM-FMF. Therefore, a new approach for measuring the DMGD in the PM-FMF 42 needs to be developed. 43

In this work, two new schemes are proposed, for the first time to our knowledge, to measure the DMGD and the mode field in the PM-FMF, based on the modification of the S² method. In the former scheme, a polarizer is added to control the polarization state of the incident light. When only X- or Y-polarized light is fed into the fiber, the LP_{01x} mode or LP_{01y} mode can be chosen as the dominant mode, and all modes in a single measurement can meet the condition of 47

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light interference. Using this method, we need two measurements to complete the assessment of all LP modes. In the 48 latter scheme, two polarizers are added in the conventional S² setup. The first polarizer is used to control the power 49 ratio between the two polarization states, after the incident light enters the PM-FMF. The second polarizer is to control 50 the polarization direction of the emitted light. Therefore, the LPoly mode can be chosen as the dominant mode among 51 all LP modes in two directions when the power of the Y-polarized ray is much higher than the power of the X-polarized 52 ray. This can be controlled by polarizer 1. The interference equation of S^2 can then be applied since the output light of 53 all modes has the same polarization direction. Results of the above two measurement schemes show a good agreement 54 between each other. 55

2. Principle and Experimental Setup of S² Imaging

S² imaging, a typical measurement technique for characterizing fibers, based on spatially resolved spectral interference which occurs when the light in an FMF is scattered into different modes [6]. These modes propagate with different group delays. In the first method, when only X-polarized light enters the PM-FMF, we assume to have two modes: a fundamental mode LP_{01x} and a high-order mode (HOM). Their spatially- and frequency- dependent amplitudes are $A_{1x} (x,y,\omega)$ and $A_{2x} (x,y,\omega)$, respectively, which are linked via a wavelength-independent constant $\alpha(x,y)$, e.g. see in [5]

$$I_{2X}(x, y, \omega) = \alpha^2(x, y)I_{1X}(x, y, \omega)$$
(1) 62

If the DMGD is assumed to be independent of frequency, the spectral intensity caused by the interference between 63 two modes can be written as 64

$$I_X(x, y, \omega) = I_{1X}(x, y, \omega) [1 + \alpha^2(x, y) + 2\alpha(x, y)\cos(\tau_b \omega)]$$
(2) 65

where τ_b is the period of the beat (caused by the DMGD) frequency between two modes. The Fourier transform of the spectral intensity is then 67

$$B_X(x, y, \tau) = [1 + \alpha^2(x, y)]B_{1X}(x, y, \tau) + \alpha(x, y)[B_{1X}(x, y, \tau - \tau_b) + B_{1X}(x, y, \tau + \tau_b)]$$
(3) 68

where $B_{1x}(x,y,\tau)$ is the Fourier transform of the optical spectrum of the LP_{01x} mode. For PM-FMFs with more than two modes in the X-polarization direction, the interference would occur between each individual mode. This will affect the measurement of the DMGD. By providing a much stronger excitation of one mode than that of all other modes at the input side, the interference between the dominant mode and a weak mode will eclipse the interference between any two weak modes [14]. Equations and the principle of the Y-polarized light can be described similarly to the X-polarized light. The schematic of the S² measurement system using the first approach is shown in Fig. 1.



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Figure 1. Schematic of the S² PM-FMF testbed using the first approach. FC: fiber collimator; L: lens.

Since the laser tuning works much faster than the point-to-point image scanning in the optical spectrum analyzer (OSA), in this experiment, we have employed the tunable laser source (TLS) as the light source and the charge coupled 78 device (CCD) camera as the receiver to detect the entire spatial distribution of the light intensity. The TLS is used to 79 produce the light wave centered at a certain frequency with the predefined tuning range and interval. The variable 80 optical attenuator (VOA) is employed to control the intensity of the incident light (into the fiber), in order to protect the 81 photodetector in the camera and to produce more accurate measurement results. The polarizer is to generate and 82

manage the linearly polarized light. The polarization of the light wave is controlled to be identical as the principal axis 83 of the PM-FMF, so that only modes in X-polarization (or Y-polarization) can pass through the fiber. A splice with offset 84 is implemented between the single-mode fiber (SMF) and the fiber under test (FUT) in order to excite multiple HOMs. 85 The LP01x mode or LP01y mode is set as the dominant mode. At the output end of the FUT, the beam is expanded using 86 a series of lenses and is projected onto the camera. The neutral-density filters (NDF) is used to control the intensity of 87 the optical beam to avoid saturating the detector. A shielding device (SD) is applied to mitigate the electromagnetic 88 disturbance in front of the CCD camera. During the experiment, the CCD camera can collect the profiles of the output 89 mode fields (at different frequencies), when the TLS is operated at the frequency sweeping mode. The data obtained by 90 CCD are processed off-line using the computer and the final S² measurement results will be obtained. 91



Figure 2. Schematic of the S² PM-FMF testbed using the second approach

Using the above structure in Fig. 1, the results will be measured when the X- and the Y-polarized light are fed into 94 the fiber, respectively. This means that two measurements will be required to obtain a whole set of results. To measure 95 DMGD values of all LP modes simultaneously, the polarization direction of the incident light should have components 96 in both X- and Y-directions and the polarization direction of each mode in the output light should be identical. The 97 block diagram of the S² measurement system using the second scheme is shown in Fig. 2. Polarizer 1 is again applied to 98 generate and control the linearly polarized modes. Here polarizer 1 leaves an angle between linearly polarized modes 99 and the principal axis of the PM-FMF to ensure the simultaneous transmission of X-pol and Y-pol modes through fibers. 100 The power of the Y-polarized ray is much higher than that of the X-polarized ray under the control of polarizer 1. 101 Thereby the LPoly is set as the dominant mode. Polarizer 2 is employed to project all modes (output from FUT) onto the 102 same polarization direction to satisfy the condition of interference. In terms of the system complexity, the second scheme 103 only requires one additional polarizer, while it can achieve a simultaneous measurement of all LP modes. 104

3. Experiments and Results

The FUT in the experiment is a panda-type PM-FMF with a length of 10 m. We first use the experimental testbed 106 shown in Fig. 1 to measure the S² results when only the X- or the Y-polarized light passes through the fiber. The tuning 107 range of the TLS is from 192268 GHz to 194828 GHz and the tuning interval is set as 5 GHz. The CCD camera acquires 108 images of the output light intensity as the TLS frequency is tuned. The total number of the images collected is 512. In 109 the experiment where only X-polarized light enters the fiber, the DMGDs of all modes in the X-polarized light is 111 can be obtained by taking the Fourier transform of the intensity spectrum. The S² result for the X-polarized light is 111 shown in Fig. 3.

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Figure 3. DMGD and mode field measurement results for the X-polarized light.

In Fig. 3, there are clearly several different discrete peaks, corresponding to interference between the fundamental 115 LP_{01x} mode and HOMs. The DMGDs of LP_{11ax} and LP_{11bx} relative to LP_{01x} are calculated as 3.672 ps/m and 3.984 ps/m, 116 respectively. Then for the experiment where only Y-polarized light enters the fiber, the S² result is shown in Fig. 4. The DMGDs of LP_{11ay} and LP_{11by} relative to LP_{01y} are calculated as 3.672 ps/m and 3.984 ps/m, respectively. 118



Figure 4. DMGD and mode field measurement results for the Y-polarized light.

Using the S² system provided in Fig. 2, we can complete the measurement of all LP modes in a single test. The 121 DMGD and mode field measurement results are shown in Fig. 5. It can be seen from Fig. 5 that the DMGD values of 122 LP01x, LP11ay, LP11by, LP11ax and LP11bx, relative to LP01y, are 1.914 ps/m, 3.672 ps/m, 3.984 ps/m, 5.547 ps/m and 5.938 ps/m, 123 respectively. That is, the DMGDs of LP_{11ay} and LP_{11by}, relative to LP_{01y}, are 3.672 ps/m and 3.984 ps/m, the DMGDs of 124 LP_{11ax} and LP_{11bx}, relative to LP_{01x}, are 3.633 ps/m and 4.024 ps/m. Comparing the results from the two methods, the 125 DMGD values of LP11ay and LP11by are exactly the same, and the DMGD values of LP11ax and LP11bx are slightly different 126 by -0.039 ps/m and 0.040 ps/m, respectively. The accuracy of the two method is over 98.9%. Therefore, the measurement 127 results from these two methods show good agreement, and this indicates that it is feasible to use the proposed two 128 methods to measure the DMGD in the PM-FMF. 129

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Figure 5. DMGD and mode field measurement results using the second scheme.

4. Conclusions

In this work, we have developed two new methods to measure the DMGD in the PM-FMF. It has been experimen-133 tally demonstrated that both appraoches can accurately estimate the DMGD in the PM-FMF, and measurement results 134 from the two schemes show a good agreement. These two methods make up for shortcomings of the traditional S² 135 method, in which the dominant mode cannot be determined. The former scheme selects a dominant mode for each 136 polarization direction, and the latter scheme employs the LP01y mode as the dominant mode for all LP modes. Using the 137 second measurement scheme, we can achieve the measurement of all LP modes in the PM-FMF via a single test. Com-138 pared to the first approach, the second scheme can double the measurement efficiency, by adding only one polarizer. 139 Therefore, we recommend the use of the second approach to measure the DMGD in the PM-FMF when experimental 140 devices are sufficient. The characterization of fiber parameters using our proposed schemes will facilitate the design 141 and the optimization of the PM-FMF, which will play an important role in the development of optical communication 142 systems. 143

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