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# 1 Digital Light Processing 3D Printing of Lightweight Fe<sub>3</sub>O<sub>4</sub>/rGO/resin Composites with 2 Enhanced Microwave Absorption

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7 **Abstract:** A Fe<sub>3</sub>O<sub>4</sub>/rGO reinforced photocurable resin composite with gyroid structure was firstly fabricated by digital  
8 light processing (DLP) 3D printing. The obtained gyroid template was further coated with absorbants and experienced a  
9 post-curing treatment for microwave absorption (MA) applications. The minimum reflection loss of the Fe<sub>3</sub>O<sub>4</sub>/rGO/resin  
10 gyroid composite coated with Fe<sub>3</sub>O<sub>4</sub>/rGO nanoparticles reached -38 dB at 10.8 GHz and a thickness of 2.5 mm, while  
11 effective absorption band was 77% in the X-band, exhibiting the best MA performance. The leverage of DLP 3D printing  
12 allows for an optimal structure for absorbants coating and increases the opportunity for electromagnetic wave  
13 reflection/refraction/transmission. The synergistic effects of hybrid Fe<sub>3</sub>O<sub>4</sub>/rGO/resin template coated with Fe<sub>3</sub>O<sub>4</sub>/rGO and  
14 gyroid structure effectively promote the MA performance and realize the manufacturing of lightweighting composites for  
15 future electromagnetic protection applications.

16 **Keywords:** 3D printing, composite materials, digital light processing, Fe<sub>3</sub>O<sub>4</sub>/rGO, microwave absorption, gyroid  
17 structure.

## 18 1. Introduction

19 With the rapid development of electromagnetic technology, the accompanying intensified electromagnetic pollution has  
20 drawn increasing attention [1]. Microwave absorption (MA) materials, with a wide absorption band and strong absorption  
21 ability, are promising materials for applications that need to shield and absorb the electromagnetic radiation and interface  
22 in undesired bandwidths [2]. Fe<sub>3</sub>O<sub>4</sub> nanoparticles have been widely considered for their high magnetic saturation strength  
23 and magnetic loss ability, however, agglomeration in liquids and resins, and poor electrical conductivity greatly constrain

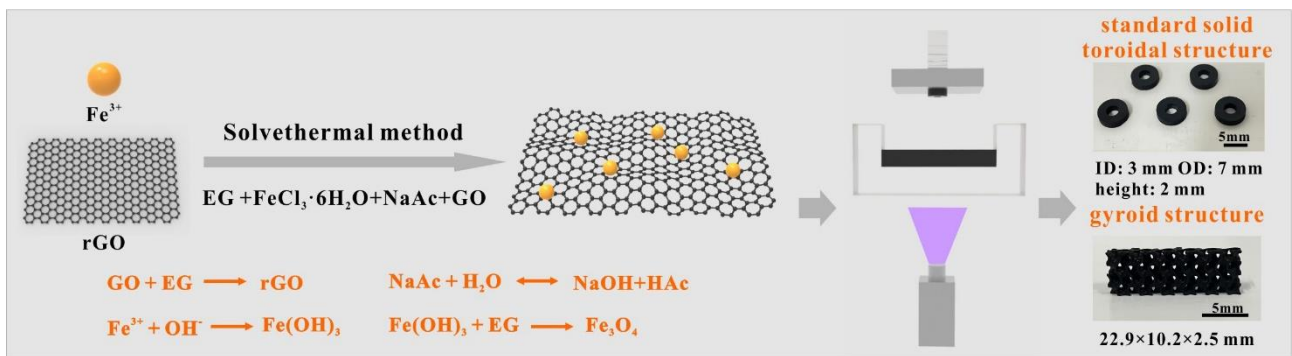
1 its use in further applications [3, 4]. To tackle this problem, reduced graphene oxide (rGO) is currently being considered  
2 as an alternative choice in combination with Fe<sub>3</sub>O<sub>4</sub> to enhance the electromagnetic MA performance of composites due  
3 to its high surface area, high charge carrier mobility, ultra-low density, and excellent electrical conductivity [5-7]. To date,  
4 some novel Fe<sub>3</sub>O<sub>4</sub>/rGO composite absorbers such as hierarchical porous Fe<sub>3</sub>O<sub>4</sub>/rGO [8], Fe<sub>3</sub>O<sub>4</sub> flakes/rGO [9], and Fe<sub>3</sub>O<sub>4</sub>  
5 hollow nanoflowers/rGO [10] with excellent MA performance have been successfully synthesized. However, these  
6 interesting MA materials still have seen limited applications due to their high weight and narrow absorption bandwidth  
7 [11]. Special design structures can make up for these drawbacks and have achieved excellent electric and magnetic loss  
8 properties, attributing to electromagnetic resonance and coupling effects [12, 13]. Due to the limitation of traditional  
9 material processing procedures (e.g., molding, hot-pressing, sintering and binding), only simple geometrical structures  
10 can be developed such as sandwich and honeycomb structures [14-16]. Digital light processing (DLP) 3D printing  
11 technology opens up new avenues to realize more complex structures with stronger MA performance, wider bandwidths  
12 and lightweighting by a combination of MA structure and material compositional design for higher resolution, precision,  
13 and customized complex designs. It adopts a layer-to-layer strategy with the projector – the designed pattern of each layer  
14 is projected, which improves the surface profile, surface roughness, and high printing efficiency [17].

15 In this study, Fe<sub>3</sub>O<sub>4</sub>/rGO nanoparticles fabricated via an *in-situ* reduction one-step solvothermal process were firstly DLP  
16 3D printed using a photocurable resin. The printed gyroid structure acted as a template for maximum specific surface area,  
17 by regulating the infiltration of various absorbants in the template. The design of structure, material composition and  
18 absorbants coating allows for an enhancement in absorption bandwidth, reflection loss ( $R_L$ ), and lightweighting, thus  
19 opening up potential applications in future MA devices.

## 20 **2. Experimental**

21 The synthesis process was illustrated in Fig. 1, 400 mg GO (JCNO Technology Co. Ltd, China, diameter: 0.5-3  $\mu$ m,  
22 thickness: 1 nm, monolayer rate: >91%) was dispersed in ethylene glycol (EG, C<sub>2</sub>H<sub>6</sub>O<sub>2</sub>, AR, 10009818) accompanied  
23 by ultrasonication treatment (Lawson DH92-IIN, China). 10 g FeCl<sub>3</sub>·6H<sub>2</sub>O, 35 g NaAc powder and 5 g polyethylene

1 glycol 1000 (PEG 1000) were dissolved into EG for 1 h by mechanical stirring to produce a yellow-brown liquid.  
 2 Subsequently, the two mixtures were transferred into Teflon-lined stainless-steel autoclaves for solvothermal reaction at  
 3 180°C for 12 h. The produced black precipitates were collected, washed, and dried.  
 4 The fabrication of photocurable resin (including a biodegradable PLA-PUA monomer, TEGDMA diluent and Irgacure  
 5 819 photoinitiator, in a 58:39:3 wt ratio) was reported in detail in our previous work [18]. The gyroid templates were DLP  
 6 3D printed using a 30 wt.% Fe<sub>3</sub>O<sub>4</sub>/rGO/resin suspension and further infiltrated in Fe<sub>3</sub>O<sub>4</sub>/rGO (50 wt.%) suspension and  
 7 rGO suspension (4 wt.%), respectively, increasing the nanoparticle loading to 40 wt.% and 4 wt.%, respectively, after  
 8 drying.



9  
 10 **Fig. 1.** Schematic of synthesis and DLP 3D printing process.

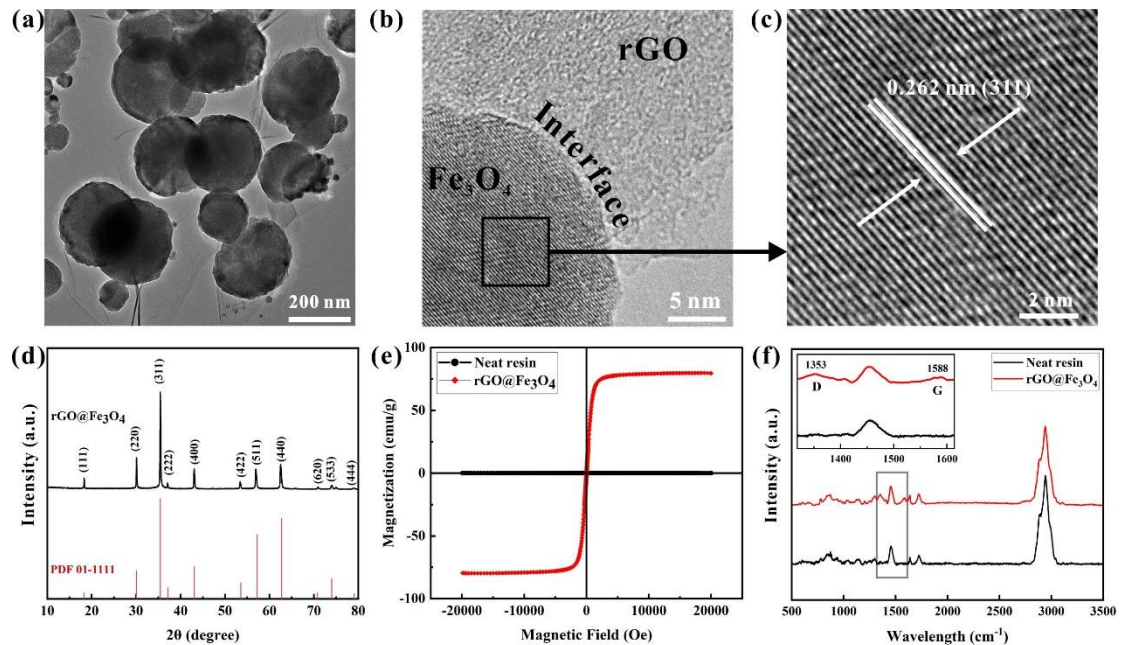
11 The morphology and structure of Fe<sub>3</sub>O<sub>4</sub>/rGO nanoparticles were characterized by transmission electron microscope (TEM,  
 12 TF20). The 3D printed samples were measured by X-ray diffraction (XRD, D8 Advance 25), Raman spectroscopy (532  
 13 nm excitation laser, Horiba Scientific), and vibrating sample magnetometer (LakeShore7404). Electromagnetic  
 14 parameters were measured by a vector network analyzer (VNA, Agilent E5071C), the printed toroidal samples were tested  
 15 in the range of 1-18 GHz at room temperature (RT) using a coaxial method and the printed gyroid structures were tested  
 16 in the range of 8.2 to 12.4 GHz (X-band) using a waveguide method.

### 17 **3. Results and discussion**

18 Spherical Fe<sub>3</sub>O<sub>4</sub> nanoparticles were uniformly wrapped by 2D rGO nanosheets, producing multiple interfaces (Fig. 2a-b).

19 Fig. 2c further shows an HRTEM image of Fe<sub>3</sub>O<sub>4</sub>/rGO, and the lattice fringes with an interplanar spacing value of 0.262

1 nm, related to the (311) planes of  $\text{Fe}_3\text{O}_4$ . Typical XRD diffraction peaks (Fig. 2d) of the 3D printed  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$   
 2 composite at  $18.28^\circ$ ,  $30.06^\circ$ ,  $35.45^\circ$ ,  $37.12^\circ$ ,  $41.04^\circ$ ,  $53.55^\circ$ ,  $57.17^\circ$ ,  $62.73^\circ$ ,  $70.78^\circ$ ,  $74^\circ$  and  $79.08^\circ$  reflected the cubic  
 3 crystal structure of  $\text{Fe}_3\text{O}_4$  (PDF 01-1111) [19], indicating that the crystal structure of  $\text{Fe}_3\text{O}_4$  was successfully obtained in  
 4 the solvent thermal method without damage induced to the crystal structure during the printing process. The absence of  
 5 the rGO peak in the XRD pattern causing by the crystallization of  $\text{Fe}_3\text{O}_4$  in the rGO interlayer destroyed the ordered  
 6 interlayer structure of rGO. The magnetic behavior of neat resin (Fig. 2e) was almost a straight line, reflecting that there  
 7 was no ferromagnetic behavior, while the hysteresis curve of the 3D printed  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite exhibited a  
 8 typical S-like shape, with a saturation magnetization ( $M_S$ ) value of 78.32 emu/g, indicating that it was superparamagnetic  
 9 at RT. The Raman spectrum (Fig. 2f) detected a weak signal of rGO (D peak at  $1353\text{ cm}^{-1}$ , G peak at  $1588\text{ cm}^{-1}$ ). The  
 10 value of  $I_D/I_G$  indicated the disordering degree of the rGO, the ratio of the printed sample was 1.023, indicating that the  
 11 graphitization of graphene was consistent with graphene made by Hummer's method after a reduction treatment [20].



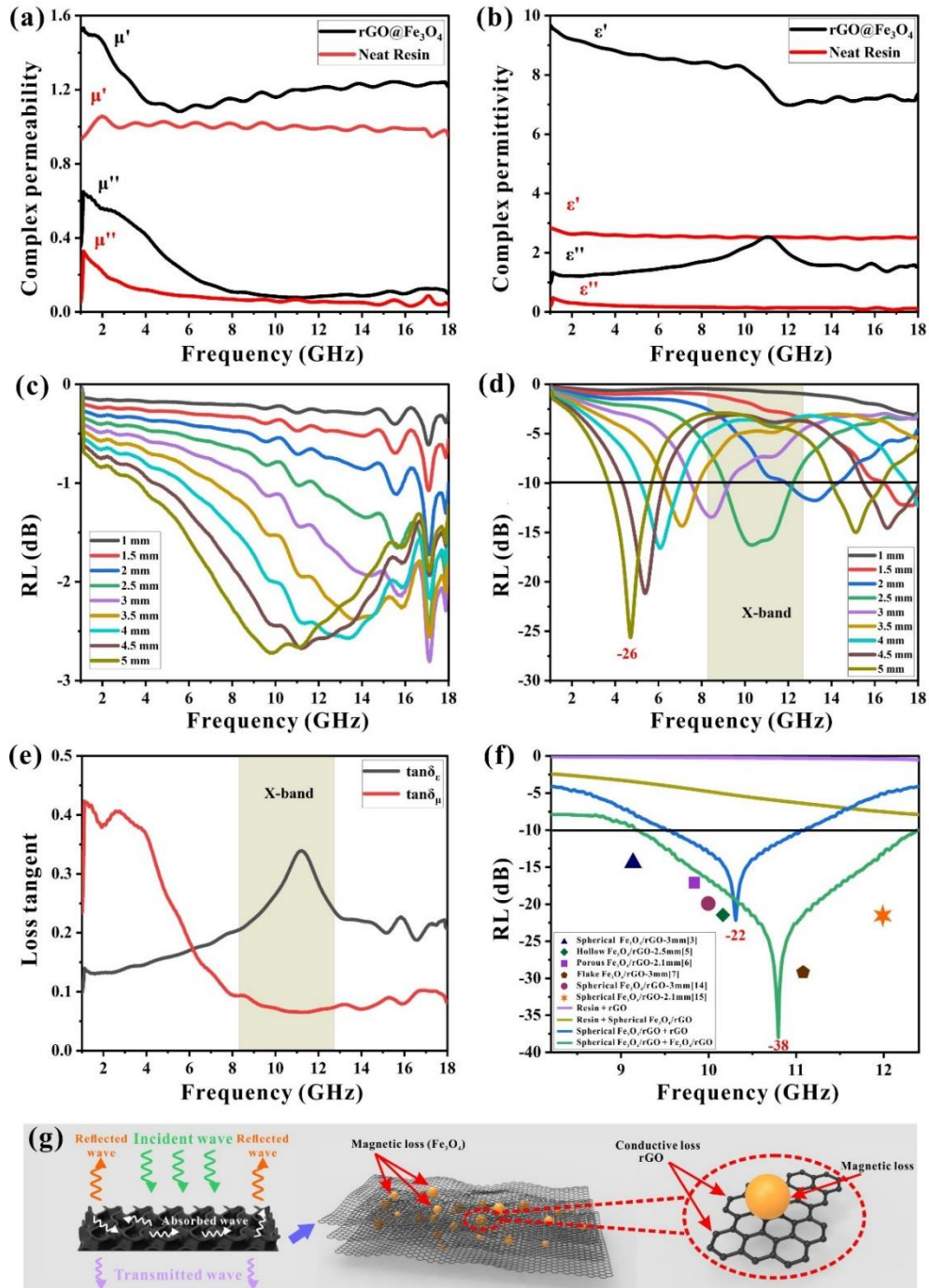
12  
 13 **Fig. 2.** (a-c) TEM images of synthesis of  $\text{Fe}_3\text{O}_4/\text{rGO}$  powder; (d) XRD patterns of the 3D printed the  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$   
 14 composite; (e) RT magnetic hysteresis loops and (f) Raman spectrum of the 3D printed composite and neat resin.

15 With the addition of  $\text{Fe}_3\text{O}_4/\text{rGO}$  nanoparticles in resin, both the real part ( $\epsilon'$ ,  $\mu'$ ) and the imaginary part ( $\epsilon''$ ,  $\mu''$ ) values of  
 16 complex permeability and permittivity of the printed  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite increased over the whole tested range

1 (Fig. 3a-b), which presented the storage ability of magnetic and electronic energy [21].  $R_L$  value was adopted to evaluate  
2 the MA performance of the samples. Based on transmit-line theory, the  $R_L$  could be calculated by following  
3 equations:  $Z_{in} = Z_0 \sqrt{\frac{\mu_r}{\epsilon_r}} \tan h[(j2\pi f d/c) (\mu_r \epsilon_r)^{\frac{1}{2}}]$  and  $R_L(\text{dB}) = 20 \log \left| \frac{Z_{in}-1}{Z_{in}+1} \right|$ .

4 Fig. 3c-d showed  $R_L$  values of DLP 3D printed neat resin and  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite of different thickness in the  
5 range of 1 to 18 GHz. The addition of  $\text{Fe}_3\text{O}_4/\text{rGO}$  greatly influenced the MA performance. The  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite  
6 had a minimum  $R_L$  (-26 dB at 4.73 GHz at a layer thickness of 5 mm), while the effective absorption bandwidth (<-10  
7 dB) could reach 3.17 GHz (9.05-12.22 GHz) at a thickness of 2.5 mm. The attenuation ability of dielectric and magnetic  
8 absorption were described by the dielectric loss tangent ( $\tan \delta_\epsilon = \epsilon''/\epsilon'$ ) and magnetic loss tangent ( $\tan \delta_\mu = \mu''/\mu'$ ) (Fig.  
9 3e). Obviously both the dielectric and magnetic loss existed over the whole test range in the printed  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$   
10 composite, exhibiting typical magnetic resonance at 1-6 GHz, and the dielectric loss plays a more important role than  
11 magnetic loss in dissipating electromagnetic wave in the X-band ( $\tan \delta_\epsilon = 0.21-0.34$ ) [21, 22]. To further leverage the  
12 composites with excellent MA performance in the X-band, gyroid structures with a high surface area were printed as  
13 templates in a thickness of 2.5 mm (neat resin and  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite). There was no MA performance  
14 improvement when using the neat resin as a template even coated with rGO or  $\text{Fe}_3\text{O}_4/\text{rGO}$  (Fig. 3f). In contrast, the  
15  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  template infiltrated with  $\text{Fe}_3\text{O}_4/\text{rGO}$  suspension and post-cured displayed enhanced MA performance  
16 and a minimum  $R_L$  was reached at -22 and -38 GHz after infiltration with rGO and  $\text{Fe}_3\text{O}_4/\text{rGO}$  suspensions, respectively.  
17 It was also worth noting that the bandwidth exceeding -10 dB was 3.24 GHz (9.16-12.4 GHz), reaching 77% absorption  
18 band in the X-band after the  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  template was coated with  $\text{Fe}_3\text{O}_4/\text{rGO}$ , displaying the best MA performance  
19 compared with 30-40 wt.%  $\text{Fe}_3\text{O}_4/\text{rGO}$  composites (The mass fraction of powder in the paraffin wax) from literature (Fig.  
20 3f). Fig. 3g further elaborates on the possible MA mechanism of composite with gyroid structure. Firstly, the introduction  
21 of a gyroid template structure increased the number of multiple reflections and scattering at the surface or inside the  
22 structure for microwaves. Secondly, the gyroid template provided a maximum surface area for nanoparticles coating, and  
23 this structural advantage effectively compensated for low concentration of graphene that could be introduced into

1 photocurable resin due to the absorption of UV light. Thirdly, with the addition of  $\text{Fe}_3\text{O}_4/\text{rGO}$  nanoparticles, both the  
 2 dielectric and magnetic loss ability are significantly enhanced, thereby favouring MA capability. Finally, the large number  
 3 of rGO-rGO and rGO- $\text{Fe}_3\text{O}_4$  interfaces induced a strong interfacial polarization and associated relaxation effect,  
 4 enhancing the attenuation capability of the composite and facilitates the conversion of electromagnetic energy into thermal  
 5 energy.



6  
 7 **Fig. 3.** (a) The complex permeability and (b) complex permittivity of  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite and neat resin with

1 toroidal structure; the  $R_L$  of (c) neat resin and (d)  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite; (e) loss tangent of  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$   
2 composite; (f)  $R_L$  values of the obtained composites and results from literature [4, 6, 9, 19, 20]; (g) Schematic diagram of  
3 MA mechanism.

#### 4 **4. Conclusion**

5 A novel strategy was developed by leveraging a DLP 3D printed gyroid structure with the unique MA property of hybrid  
6  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$  composite with various absorbants coating to obtain a satisfactory absorption bandwidth in the X-band  
7 and enhanced MA performance, while simultaneously reducing thickness and realizing lightweight. The  $\text{Fe}_3\text{O}_4/\text{rGO}/\text{resin}$   
8 gyroid template coated with  $\text{Fe}_3\text{O}_4/\text{rGO}$  nanoparticles displayed a minimum  $R_L$  of -38 dB at a thickness of 2.5 mm with  
9 an effective bandwidth (9.16-12.4 GHz), covering 77% in the X-band.

#### 10 **Acknowledgements**

11 The work was financially supported by National Natural Science Foundation of China (No.51902295), Applied Basic  
12 Frontier Research of Wuhan Municipal Science and Technology Bureau (No.2019020701011454) and Hubei Province  
13 Natural Science Foundation grant (No. 2019CFB264).

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